NOISE IMPACT ASSESSMENT

DALC
Developer and Landlord Certification

105-111 Winchester Road, Chandlers Ford, Hampshire SO53 2ZA

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Chartered Institute of Environmental Health

IEngineer

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This report has been compiled by Deane Austin Ltd (DAA) with all reasonable skill, care and diligence in accordance with generally accepted acoustic consultancy principles. Information contained in this document contains confidential and commercially sensitive information and shall not be disclosed to third parties.				

1.0 INTRODUCTION

DAA Group has been appointed to carry out a Noise Impact Assessment at 105-111 Winchester Road, Chandlers Ford, Hampshire SO53 2ZA to support a Planning Application for the addition of a 2nd floor to the front elevation.

Using results of the noise survey, the sound insulation performance for the whole building envelope including glazing (windows) is assessed, and a scheme of noise mitigation measures is established and included in the report verified by BS8233:2014 rigorous method building envelope sound insulation calculations.

A scheme of noise mitigation measures in the report provides specification details as appropriate for sound insulation upgrade treatment to the separating walls and separating floors.

The technical content of this assessment has been provided by a Tech member of the Institute of Acoustics.

The Institute of Acoustics is the UK's professional body for those working in acoustics, noise and vibration.

2.0 NOISE CRITERIA

2.1 NATIONAL PLANNING POLICY FRAMEWORK (NPPF)

The Department for Communities and Local Government introduced the National Planning Policy Framework (NPPF) in March 2012. The latest revision of the NPPF is dated July 2021.

The NPPF sets out the Government's planning policies for England and how these are expected to be applied. It provides a framework where local Councils can produce their own local and neighbourhood plans which reflect the needs of their communities.

In conserving and enhancing the natural environment, the planning system should prevent both new and existing development from contributing to, or being put at, unacceptable risk from environmental factors including noise.

Planning policies and decisions should aim to avoid noise giving rise to significant adverse impacts on health and quality of life as a result of new development. Conditions may be used to mitigate and reduce noise to a minimum so that adverse impacts on health and quality of life are minimised. It must be recognised that development will often create some noise and existing businesses wanting to develop in continuance of their business should not have unreasonable restrictions put on them. Reference is made within NPPF to the Noise Policy Statement for England (NPSE) as published by DEFRA in March 2021.

2.2 NOISE POLICY STATEMENT FOR ENGLAND (NPSE)

The long-term vision of the NPSE is stated within the documents scope, to 'promote good health and a good quality of life through the effective management of noise within the context of Government policy on sustainable development'. The policy aims are stated to:

- avoid significant adverse impacts on health and quality of life;
- mitigate and minimise adverse impacts on health and quality of life; and
- where possible, contribute to the improvement of health and quality of life.

The application of NPSE should mean that noise is properly taken into account at the appropriate time (for example in planning applications or appeals) where it must be considered alongside other relevant issues. The guiding principles of Government policy on sustainable development should be used to assist in the implementation of the NPSE.

The NPSE should apply to all types of noise apart from occupational noise in the workplace. The types of noises defined in the NPSE includes:

- Environmental noise from transportation sources;
- Neighbourhood noise which includes noise arising from within the community; industrial premises, trade and business premises, construction sites and noise in the street

The Noise Policy Statement England (NPSE) outlines observed effect levels relating to the above, as follows:

- **NOEL – No Observed Effect Level**

o This is the level below which no effect can be detected. In simple terms, below this level, there is no detectable effect on health and quality of life due to the noise.

- **LOAEL – Lowest Observed Adverse Effect Level**

o This is the level above which adverse effects on health and quality of life can be detected.

- **SOAEL – Significant Observed Adverse Effect Level**

o This is the level above which significant adverse effects on health and quality of life occur.

As stated in The Noise Policy Statement England (NPSE), it is not currently possible to have a single objective based measure that defines SOAEL that is applicable to all sources of noise in all situations. Specific noise levels are not stated within the guidance for this reason, and allow flexibility in the policy until further guidance is available.

2.3 ProPG: PLANNING AND NOISE

As outlined above, the National Planning Policy Framework encourages improved standards of design, although it provides no specific noise levels which should be achieved on site for varying standards of acoustic acceptability, or a prescriptive method for the assessment of noise.

ProPG: Planning and Noise was published in May 2017 in order to encourage better acoustic design for new residential schemes in order to protect future residents from the harmful effects of noise. This guidance can be seen as the missing link between the current NPPF and its predecessor, PPG24 (Planning Policy Guidance 24: Planning and Noise), which provided a prescriptive method for assessing sites for residential development, but without the nuance of 'good acoustic design' as outlined in ProPG.

ProPG allows the assessor to take a holistic approach to consider the site's suitability, taking into consideration numerous design factors which previously may not have been considered alongside the noise level measured on site, for example the orientation of the building in

relation to the main source of noise incident upon it.
It should be noted this document is not an official government code of practice, and neither replaces nor provides an authoritative interpretation of the law or government policy, and therefore should be seen as a good practice document only.

2.4 ACOUSTICS VENTILATION AND OVERHEATING

The AVO Guide includes:

* an explanation of ventilation requirements under the building regulations and as described in Approved Document F, along with typical ventilation strategies and associated noise considerations;
* an explanation of the overheating assessment methodology described in CIBSE TM59; potential acoustic criteria and guidance relating to different ventilation and overheating conditions, for both environmental noise ingress and building services noise;
* and a worked example of the application of the AVO Guide including indicative design solutions.

The AVO Guide is intended for the consideration of new residential development that will be exposed predominantly to airborne sound from transport sources, and to sound from mechanical services that are serving the dwellings in question. Although the policy coverage is limited to England, the approach may be applicable in other parts of the UK.

The AVO Guide is intended to contribute to the practice of good acoustic design, as emphasised in the Professional Practice Guidance on Planning and Noise (ProPG). In particular

2.5 BRITISH STANDARD BS 8233:2014

British Standard Code of Practice BS8233:2014 'Sound insulation and noise reduction for buildings' provides recommended guideline value for internal noise levels within dwellings which are similar in scope to guideline values contained within the World Health Organisation Guidelines for Community Noise 1999 (WHO).

Activity	Location	07:00 to23:00	23:00 to 07:00
Resting	Living room	35 dB $L_{Aeq,\ 16hour}$	
Dining	Dining room/area	40 dB $L_{Aeq,\ 16hour}$	
Sleeping (daytime resting)	Bedroom	35 dB $L_{Aeq,\ 16hour}$	30 dB $L_{Aeq,\ 8hour}$

2.4.1 Indoor ambient noise levels for dwellings

The WHO guideline noise criteria set an internal sleep disturbance noise limit of 45dB LAmax,F which should not be exceeded on a regular basis.

3.0 SITE SURVEY

3.1 SITE DESCRIPTION

The application site is situated on the first floor above Co Op Convenience Store along Winchester Road.
The area is a mix of residential and commercial properties, typical of an urban cityscape environment. The dominant noise source is traffic noise from the surrounding roads.
(See Figure 3.1)

Figure 3.1 – Proposed Site

3.2 ENVIRONMENTAL SITE SURVEY PROCEDURE

In order to characterise the sound profile of the area an environmental sound survey has been carried out from 01/12/2023 to 02/12/2023. The monitoring position was chosen in order to collect representative data for the potential noise break into the habitable rooms.
Noise Measurements were carried out 1m from the front façade on the first floor and on the roof of the proposed development at the rear. The monitoring locations are shown in Figure 3.2.

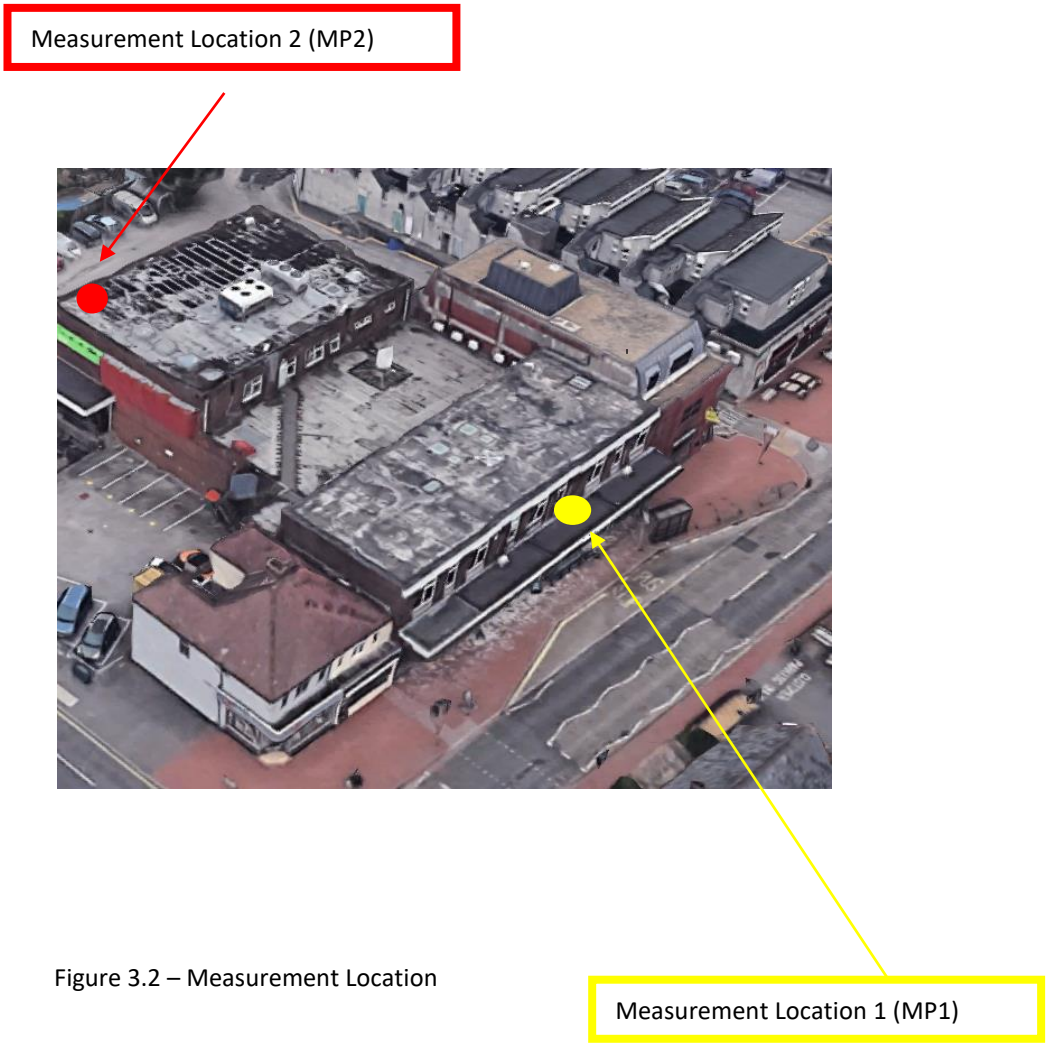


Figure 3.2 – Measurement Location

3.3 EQUIPMENT

Instrument manufacturer	Rion
Model	NA-28
Serial Number	00392485
Microphone Type	UC-59
Serial Number	14934
Calibrator	NC-74
Serial Number	34494274

Instrument manufacturer	Cirrus Research Plc
Model	IEC 61672-3:2013
Serial Number	G302987 – G303498
Microphone Type	MK:224
Serial Number	214457A
Cirrus CK: 675 Outdoor Kit	
Type 1 Acoustic Calibrator	

The calibration of the sound level meters was verified in-situ before any measurements were taken, using the hand held calibrator and reference tone of 114dB at 1kHz. Validation checks at the end of the survey indicated that all instruments had operated within permitted tolerances for drift and measured level.

Copies of Calibration certificates are available upon request.

3.4 METEOROLOGICAL CONDITIONS

As the environmental noise survey was carried out over a long un-manned period no localized records of weather conditions were taken. However, during the set up and collection of the monitoring equipment, the weather conditions have been documented in the following table. All measurements have been compared with met office weather data of the area, specifically the closest weather station, the data from the weather station is outlined in the table below. When reviewing the time history of the noise measurements, any scenarios that were considered potentially to be affected by the local weather conditions have been omitted. The analysis of the noise data includes statistical and percentile analysis and review of minimum and maximum values, which aids in the preclusion of any periods of undesirable weather conditions. The weather conditions were deemed suitable for the measurement of environmental noise in accordance with BS7445 Description and Measurement of Environmental Noise. The table below presents the average temperature, wind speed and rainfall range for each 24-hour period during the entire measurement.

Weather Conditions –Southampton Weather station				
Time Period	Air Temp (◦C)	Rainfall mm/h	Prevailing Wind Direction	Wind Speed (m/s)
01/12/2023 – 00:00 – 23:59	01 - 06	0.0	NE	0-10
02/12/2023 – 00:00 – 23:59	01- 04	0.0	N	0-9

Table 3.4 – Weather Summary

4.0 NOISE SURVEY

The following free-field sound levels have been derived for assessment of environmental noise break-in. It shall be noted that the data is 3dB below the information in Appendix A to equate from façade to free-field conditions.
A maximum value is provided for each night-time measurement period. Based on the World Health Organisation interpretation that for a noise to be regular it needs to occur several (i.e. more than two) times per hour; the LAmax(f) noise needs to be based upon an average of 10-15 events that are typical in nature. The aim of protecting against maximum noise levels is to ensure protection against typical intermittent noise levels rather than one-off events; whereby an arithmetic average of the 15 typical maximum events across each night period is used to determine values of dB LAmax(f) reported below. These have been summarised in table 4.1 below.

Measurement Data	Free Field Sound Pressure Level dB		
	MP 1		
Time	Average $L_{Aeq,15}$	Maximum $L_{AMAX,15}$	Lowest $L_{90,15}$
07:00 – 23:00	61dB	85dB	49dB
23:00 – 07:00	50dB	73dB	46dB

Measurement Data	Free Field Sound Pressure Level dB		
	MP 2		
Time	Average $L_{Aeq,15}$	Maximum $L_{AMAX,15}$	Lowest $L_{90,15}$
07:00 – 23:00	55dB	68dB	27dB
23:00 – 07:00	49dB	58dB	24dB

Table 4.1 - Measurement Levels

Leq, ff noise levels are taken as the continuous equivalent free-field sound pressure level outside the room elements under consideration. These correspond to the highest reliable readings taken for day and night periods.

Location	T	Time	Free-Field Sound Pressure Level Leq, T dB re.20µPa						
			125Hz	250Hz	500Hz	1kHz	2kHz	4kHz	A
MP1	16h	Day	66	60	59	57	52	44	61
	8h	Night	55	49	48	46	41	33	50
		Max	78	72	71	69	64	56	73
MP2	16h	Day	59	54	53	51	46	38	55
	8h	Night	54	48	47	45	40	32	49
		Max	63	57	56	54	49	41	58

Table 4.2 Summary of Highest octave -band sound levels for break in assessment

5.0 PROPOSED RESIDENTIAL UNITS – LAYOUT DESIGN

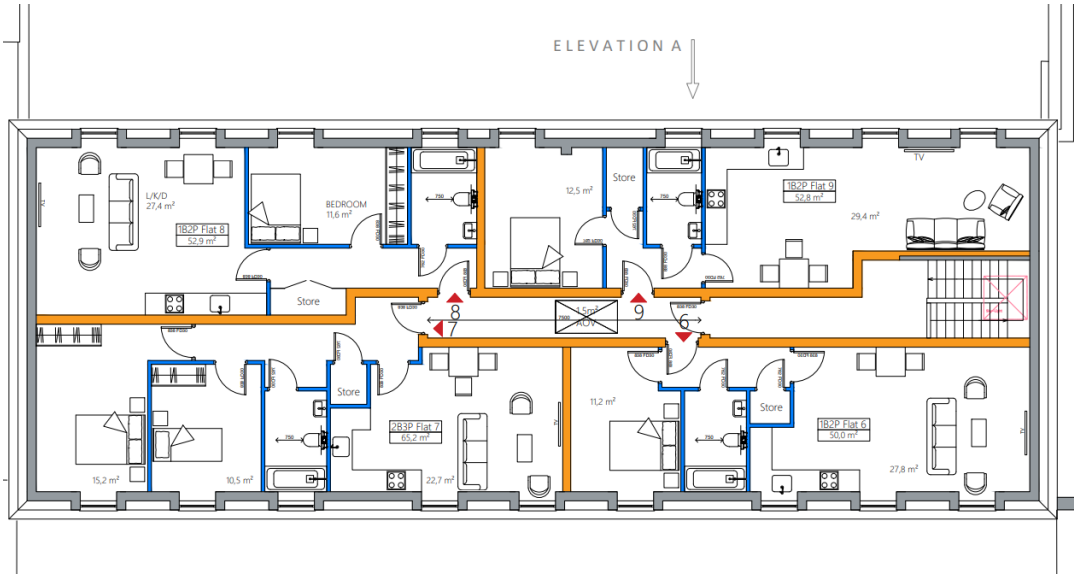


Figure 5.0 - Architectural Drawings of Proposed Front Second Floor

5.1 EXTERNAL SOUND LEVELS

It shall be read from Table 4.2 in Section 4.0 of this report, that the external sound levels taken by means of average equivalent or maximum sound levels slightly exceed the World Health Organisation requirements for external noise as described by Community Noise Guidelines (1999) in Section 2.5 of this report in the daytime at the front façade.

5.1.1 Pro PG Acoustic Design Statement

The scope of ProPG is restricted to the consideration of new residential development that will be exposed predominantly to airborne noise from transport sources. New apartments, flats and houses are the most common type of new residential development, however the guidance can also be applied to other types of residential developments such as residential institutions, care homes etc. As such it is directly applicable to this development.

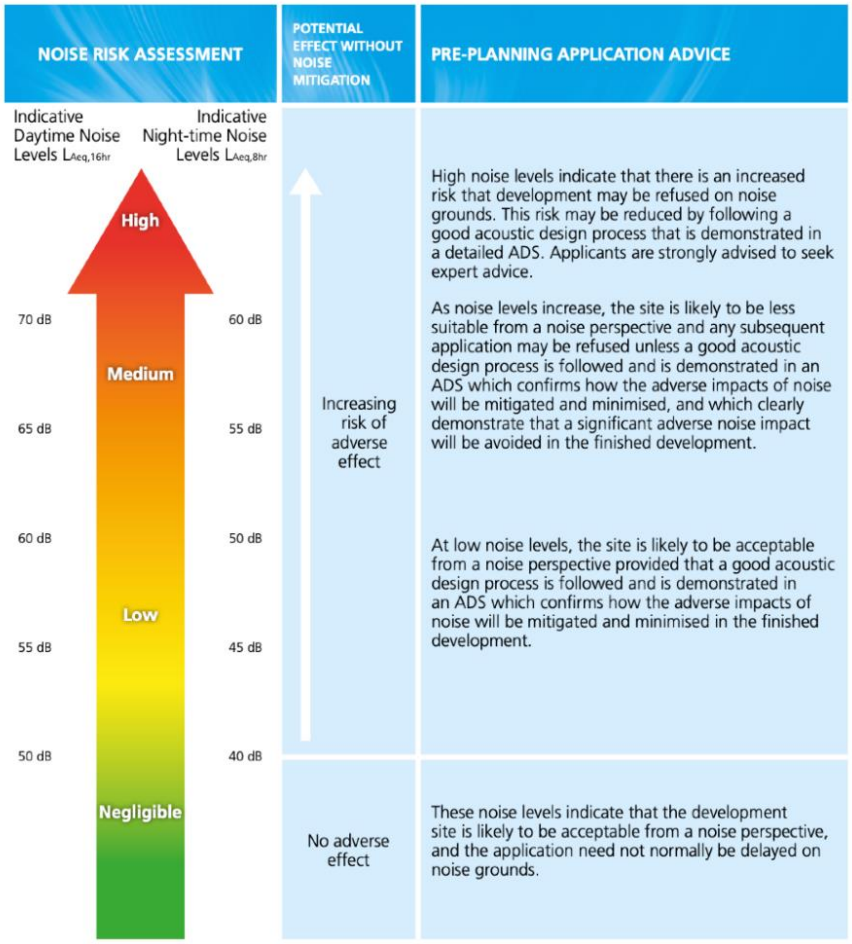


Figure 5.1 - ProPG Noise risk assessment guide

The following table assesses the ProPG noise risk for the measured data. The purpose of this is to provide a view of the noise risk at the site.

MP1	Daytime $L_{Aeq, 16hr}$ 07:00 – 23:00	Night-time $L_{Aeq, 8hr}$ 23:00 – 07:00
Noise Level	61dB	50dB
ProPG Noise Risk	MEDIUM	MEDIUM

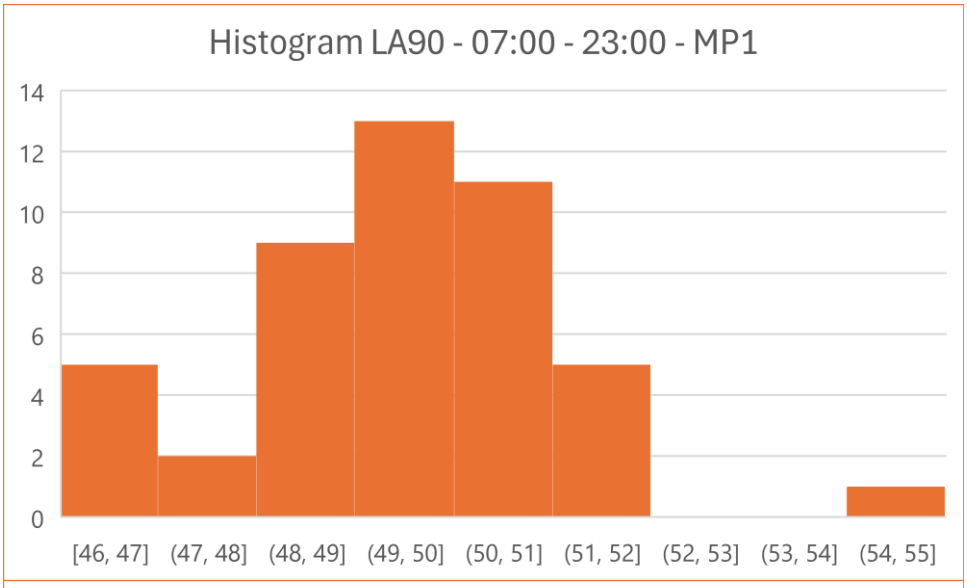
MP2	Daytime $L_{Aeq, 16hr}$ 07:00 – 23:00	Night-time $L_{Aeq, 8hr}$ 23:00 – 07:00
Noise Level	55dB	49dB
ProPG Noise Risk	LOW	LOW

Table 5.1.1 : ProPG Stage 1 Assessment table

ProPG states that "Particular care should be taken to ensure that any noise events (as quantified by LAmax,F) have been properly identified and assessed".

5.1.2 ASSESSMENT OF COMMERCIAL SOURCES

The background sound levels have been calculated in accordance with BS 4142:2014, which represents the most up-to-date guidance on the subject. Prior to the publication of the 2014 version of BS 4142, acousticians would use the lowest measured background sound levels; however, BS 4142: 2104 provides substantially more guidance on the determination of background sound levels. Section 8.1 of BS 4142: 2014 states that "for this purpose, the objective is not simply to ascertain a lowest measured background sound level, but rather to quantify what is typical during particular time periods. Among other considerations, diurnal patterns can have a major influence on background sound levels and, for example, the middle of the night can be distinctly different (and potentially of lesser importance) compared to the start or end of the night-time period for sleep purposes".
The guidance goes on to say that "a representative level ought to account for the range of background sound levels and ought not automatically to be assumed to be either the minimum or modal value".
To assess the commercial noise sources we have used the representative background noise level of 47dB and 49dB for our calculations. See histograms below:



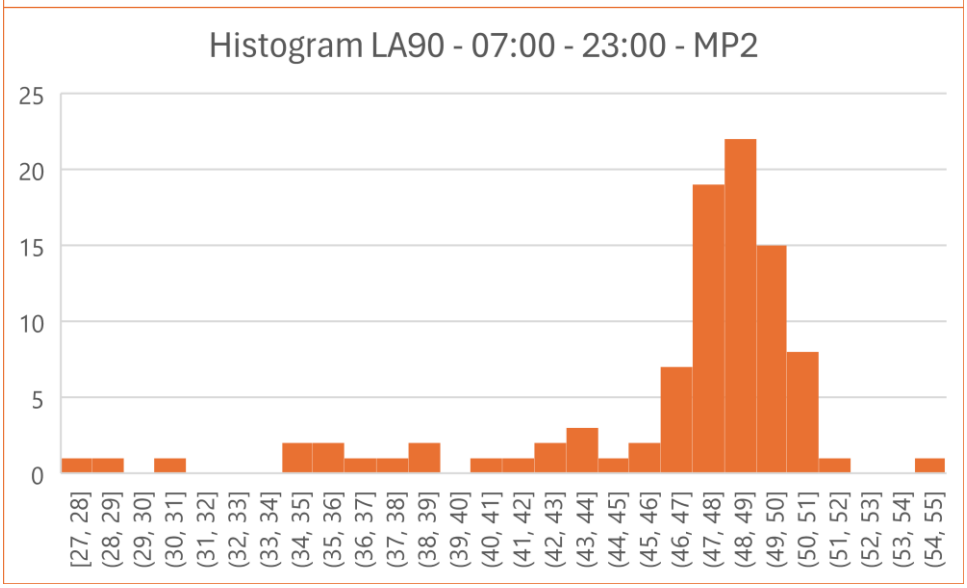


Table 5.1.2 – Background Noise Level

Where a new noise-sensitive receptor is introduced and there is extant industrial and/or commercial sound, it ought to be recognized that the industrial and/or commercial sound forms a component of the acoustic environment. In such circumstances other guidance and criteria in addition to or alternative to BS4142:2014 can also inform the appropriateness of both introducing a new noise-sensitive receptor and the extent of required noise mitigation." The observed commercial noise sources affecting the assessment areas are as follows:

	Intake/ Outlet Grilles (to be removed)
	Proposed residential Units
	5 x Fujitsu Condenser Units – AOYG09LEC
	Air Handling Unts (to be removed)
	Redundant Condenser Units
	Public House / Restaurant
	Kitchen Extraction Outlet – No. 113

Figure 5.1.2 – Commercial Noise Sources

The proposed residential units will be situated on above the Co-Op Convenience Store.
As shown in Figure 5.1.2 above. It is understood the existing plant servicing co-op will be removed.

The operating hours of Co Op are as follows:
Monday – Saturday – 07:00 – 21:00
Sundays – 10:00 – 16:00

Josies Café – adjoining the site operate as follows:
Monday – Friday – 07:30 – 17:00
Saturday – 08:00 – 17:00
Sundays – 08:00 – 16:00

Adjacent to the site is The Halfway House Public House. The Opening Hours are:
Sunday – Thursday – 11:00 – 23:00
Friday - Saturday – 11:00 – 00:00

There is no plant adjacent to the site from the pub/restaurant that could be seen/ heard. The general commercial noise will be included in the noise measurements taken at MP1. Any commercial activity from the co-op will be included in MP2 as the monitoring position was at the nearest point to the delivery area.

It is understood that the 5 Fijitsu condenser units belonging to 113 Winchester Road will be moved to their roof. See Figure 5.1.3 below.

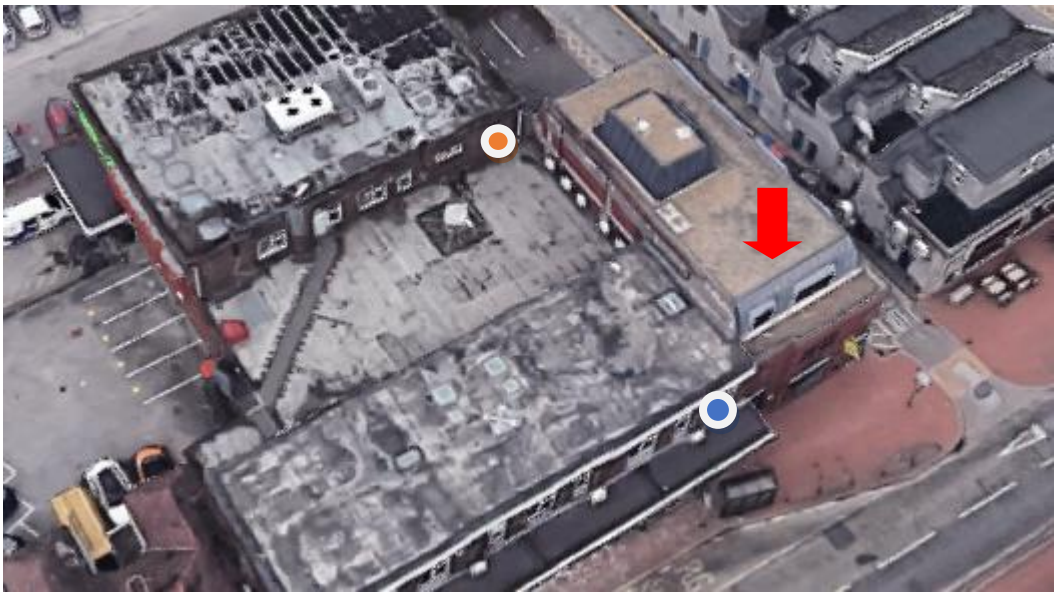


Figure 5.1.3 – Relocation of condenser units.

	Proposed NSR 1
	Proposed NSR 2
	Proposed new location of Condenser Units

6.0 BS4142:2014+A1:2019 ASSESSMENT – 1m Outside Nearest residential Window

For existing plant, the methods described in BS4142:2014 result in the following formula:
Lb=1-Log [10^(Lm/10) – 10^(Lf/10]
where
Lb = background noise level when plant is removed
Lm = background noise measured with plant running
Lf = Specific noise of the fan

The condenser units were not running during our attendance of the site, so we have used the manufacturer noise data.(See below).

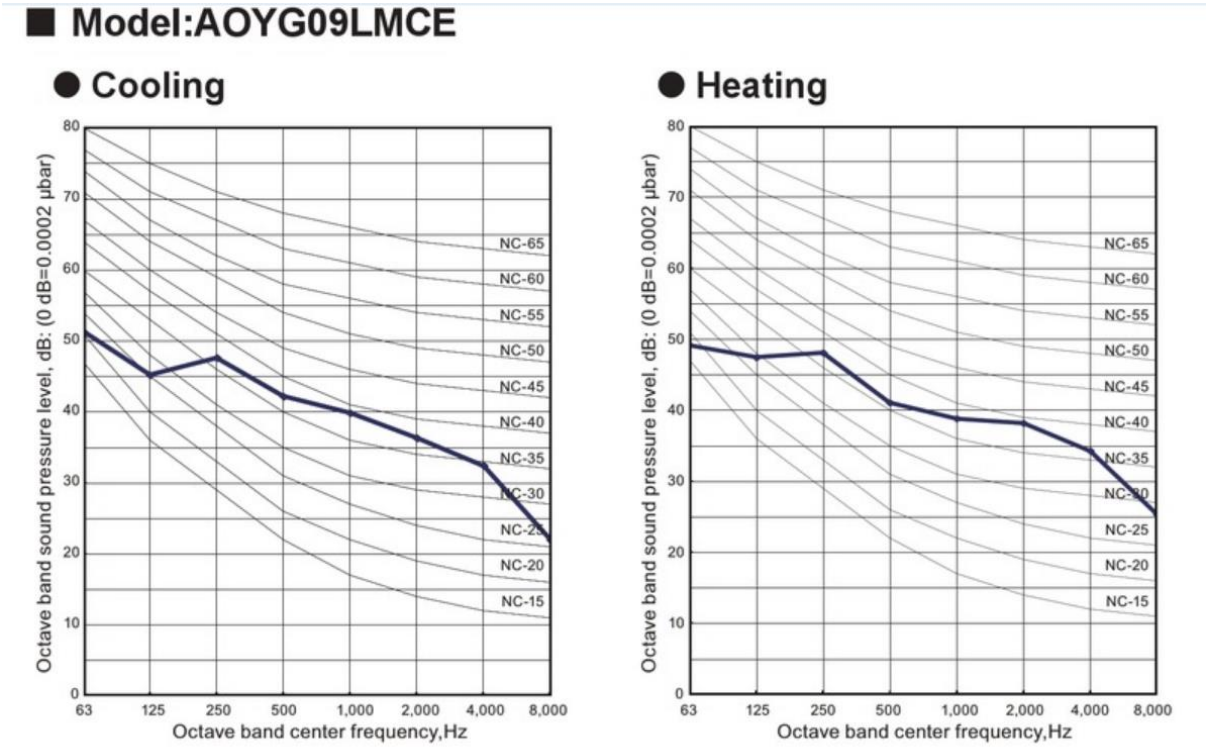


Figure 6.0 – Manufacturer Noise Data of Condenser Units – 43dB

Character corrections should be added to the 'specific sound level' if it exhibits any tonality, impulsivity, other specific characteristics and/or intermittency at the assessment location. Based on on the proposed window our measurements the plant was not tonal.

- Intermittency – We do not consider plant to have distinguishable intermittency.
- Impulsivity – Plant such as this is not normally impulsive.
- Other Sound Characteristics – we have applied a +3dB correction for other sound.

BS4142:2014 Assessment to Rear Units (MP2)	
Source Operating Period	Condenser Units 07:00 – 23:00
Reference Time Interval (Tr) Element	15 minutes Level (dB)
Specific Sound Level	23
Representative Background Noise Level (LA90)	47
Acoustic feature correction	3
Rating Level	26
Excess of Rating over Background Sound Level	-29

BS4142:2014 Assessment to Front Units (MP1)	
Source Operating Period	Condenser Units 07:00 – 23:00
Reference Time Interval (Tr) Element	15 minutes Level (dB)
Specific Sound Level	29
Representative Background Noise Level (LA90)	49
Acoustic feature correction	3
Rating Level	32
Excess of Rating over Background Sound Level	-17

Detailed calculations can be found in Appendix D.

6.1 KITCHEN EXTRACTION SYSTEM – 113 WINCHESTER RD

Figure 6.1 – Kitchen Extraction System

Noise measurements were carried out 1m outside the Proposed NSR while the fan was in operation.

	Date	Time	LAeq (dB)	LAFMax (dB)	LAF10 (dB)	LAF90 (dB)	31.5 Hz (dB)	63 Hz (dB)	125 Hz (dB)	250 Hz (dB)	500 Hz (dB)	1 kHz (dB)	2 kHz (dB)	4 kHz (dB)	8 kHz (dB)	16 kHz (dB)
Kitchen Extract on	18/02/2024	16:50	58.2	72.7	60.4	54.9	67	62.1	58.8	59	55.1	54.2	49.9	39.4	31	30.1
Kitchen Extract off	18/02/2024	17:05	54	68.3	56.3	49.9	60.5	56.3	54.4	54.2	50.3	49.3	44.6	36.5	27.1	24.8

Table 6.1 – Manned Noise Measurements

BS4142:2014 Assessment to proposed NSR	
Source Operating Period	Kitchen Extraction Unit - 113 07:30 – 17:00
Reference Time Interval (Tr)	15 minutes
Element	Level (dB)
Specific Sound Level	58
Representative Background Noise Level (LA90)	50
Acoustic feature correction	3
Rating Level	61
Excess of Rating over Background Sound Level	+11

6.2 DELIVERIES

The operators of the convenience store identify that deliveries are generally once-a-day by an articulated lorry with the delivery "window" being between 7am and 10pm on weekdays and as a result there are no specific times which can be provided in terms of exact delivery times as these vary each day within that " time window ".

6.3 109 WINCHESTER ROAD – PROPOSED STAKKS PANCAKE HOUSE

At the time of the noise assessment 109 Winchester Road was un occupied. Since then planning has been granted for a restaurant.
The proposed details are below:

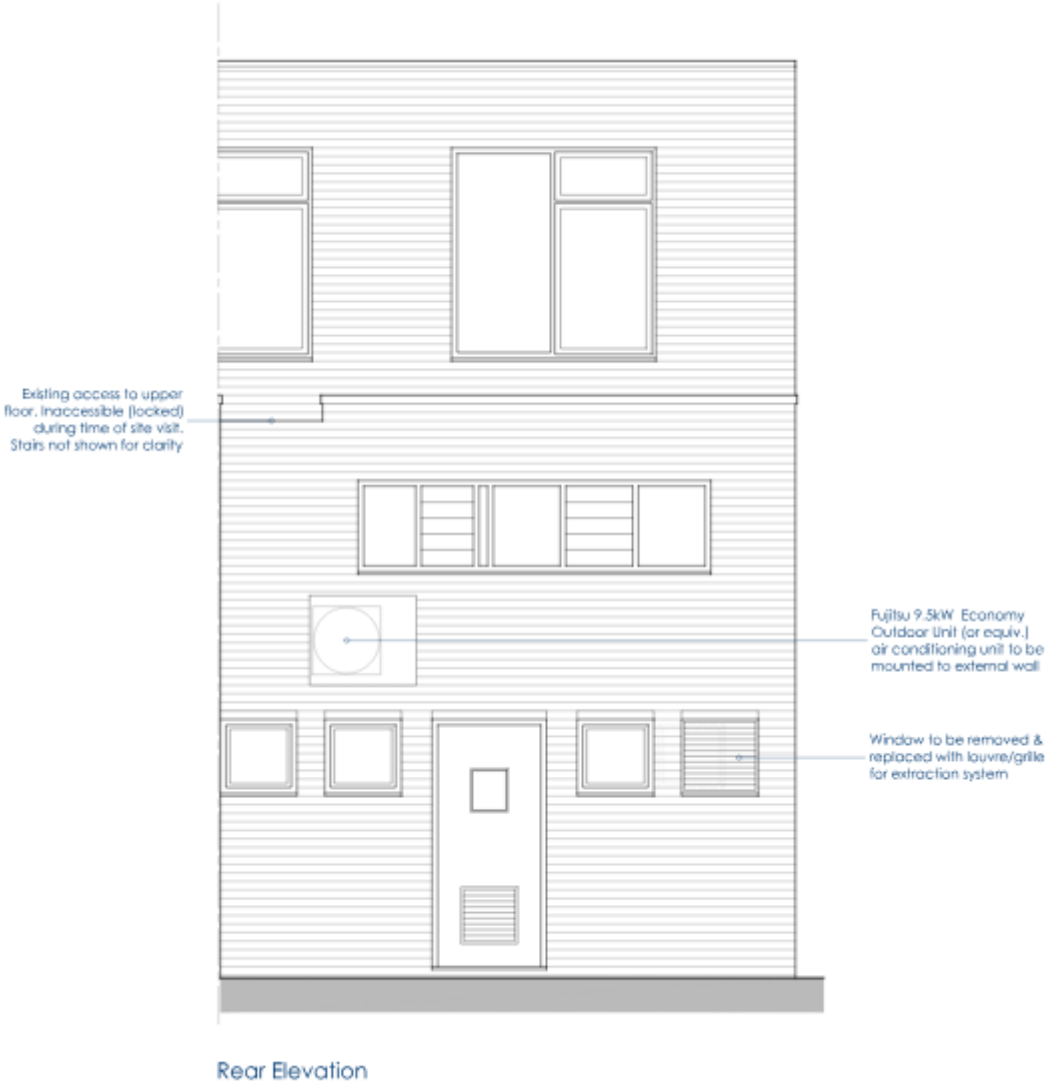


Figure 6.3 – Proposed Plans – 109 Winchester Rd.

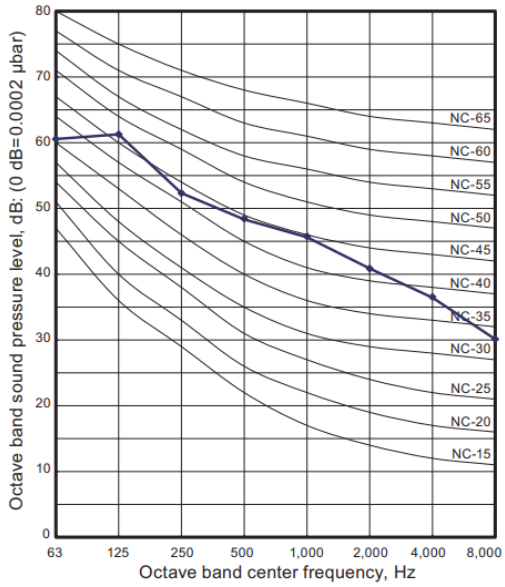
The proposed plant is an Air con unit – Fujitsu 9.5Kw and a low level extraction outlet. There are no details of the kitchen extraction system on the planning portal. We have used a typical noise level for this for our calculations.

Figure 6.3.1 – NSR to Proposed Restaurant.

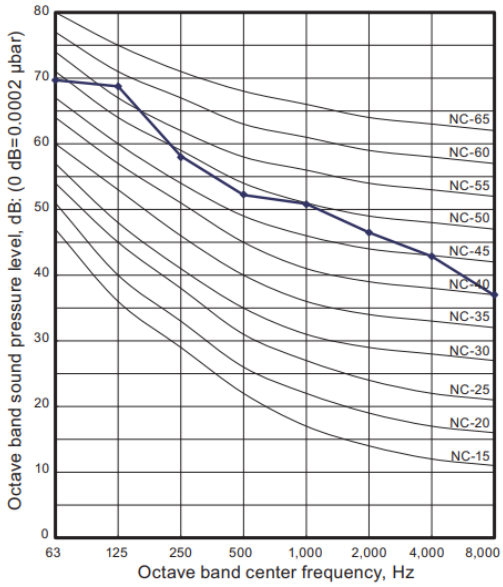
●	Proposed Condenser Unit
▭	Proposed NSR
●	Proposed Extraction Outlet

■ Model: AOYG36KBTA5

● Cooling



● Heating



Figire 6.3.2 – Noise Data – Proposed Condenser – 109 Winchester Rd.

BS4142:2014 Assessment to Proposed 109 Plant	
Source Operating Period	109 Plant 07:00 – 23:00
Reference Time Interval (Tr) Element	15 minutes Level (dB)
Specific Sound Level	38
Representative Background Noise Level (LA90)	47
Acoustic feature correction	3
Rating Level	41
Excess of Rating over Background Sound Level	-6

6.4 DISCUSSIONS AND CONTEXT

Calculations indicate the condenser units at the proposed relocated position and the proposed plant at 109 Winchester Rd. will cause no adverse effects. Regarding the kitchen flue at 113, calculations indicate that it can cause adverse effects to Flat 2 and mitigation is needed. The living area will need to have mechanical ventilation in order to negate the need to open the windows.

BS4142 states: "Where the initial estimate of the impact needs to be modified due to the context, take all pertinent factors into consideration, including the following:
The sensitivity of the receptor and whether dwellings or other premises used for residential purposes will already incorporate design measures that secure good internal and/or outdoor acoustic conditions, such as:

- Façade sound insulation treatment
- Ventilation and/or cooling that will reduce the need to have windows open so as to provide rapid or purge ventilation
- Acoustic screening." With regard to 'good acoustic conditions'

"The significance of sound of an industrial and/or commercial nature depends upon both the margin by which the rating level of the specific sound source exceeds the background sound level and the context in which the sound occur. A difference of around +10 dB or more is likely to be an indication of a significant adverse impact, depending on the context. A difference of around +5 dB is likely to be an indication of an adverse impact, depending on the context. The lower the rating level is relative to the measured background sound level, the less likely it is that the specific sound source will have an adverse impact or a significant adverse impact. Where the rating level does not exceed the background sound level, this is an indication of the specific sound source having a low impact, depending on the context."

7.0 EXTERNAL BUILDING FABRIC SPECIFICATION

Sound reduction performance calculations have been undertaken in order to specify the minimum performance required from glazed and non-glazed elements in order to achieve the recommended internal noise levels shown in Table 2.5, taking into account average and maximum noise levels monitored during the environmental noise survey.

In accordance with the assessment guidance in Annex G of BS 8233:2014, the sound insulation performance of the building can be estimated by simple calculation from the free-field noise

564CALCULATION		A	B	(A-B) +5
Location	Period	Highest Free-Field Noise Levels LAeq,T dB	BS8233/WHO Internal Noise Guidance Criteria LAeq, T dB	Typical Insulation Specification dB Rw
MP1	Day 07:00 – 23:00	61	35	31
	Night 23:00 – 07:00	50	30	26
		73	45	33
MP2	Day 07:00 – 23:00	55	35	25
	Night 23:00 – 07:00	49	30	24
		58	45	18

Table 7.0 - Sound insulation estimate using the simple calculation method of BS8233

Typical sized bedrooms with a high ratio of glazing to masonry have been used for all calculations in order to specify glazing.

As a more robust assessment, LAmax spectrum values of night-time peaks have also been considered and incorporated into the glazing calculation in order to cater for the interior limit of 45 dB LAmax for individual events, as recommended in WHO Guidelines.

7.1 NON-GLAZED ELEMENTS

It is understood that the non glazed element is brickwork cavity walls and would be expected to provide the minimum figures shown above when tested in accordance with BS EN ISO, 140-3:1995.

Element	Octave Band Centre Frequency SRI, dB					
	125	250	500	1K	2K	4K
Non-Glazed Element SRI	41	43	48	50	55	55

Table 7.1 Non-glazed elements sound reduction minimum performance

7.2 SPECIFICATION OF GLAZED UNITS

The minimum sound reduction index (SRI) value required for the glazed elements is shown in Table 7.2 & 7.2.1

Glazing Configuration – 5mm/ 14mm / 6mm							
Frequency, Hz/dB					Rw	Rw + C	Rw +Ctr
125	250	500	1K	2K	**34**	-1	-4
28	24	29	41	37			

Table 7.2 – Required Glazing Performance front façade and Flat 2 Living Area.

Glazing Configuration – 3mm/ 10mm cavity/3mm							
Frequency, Hz/dB					Rw	Rw + C	Rw +Ctr
125	250	500	1K	2K	**29**	-1	-4
14	19	24	31	41			

Table 7.2.1 – Required Glazing Performance rear façade.

Alternatively, the existing glazing could be retained and add a secondary 4 mm pane of glass, with a minimum 100 mm cavity to the existing glazing. This would provide 43dB Rw. (See appendix D).

The sound reduction performance stated above must be achieved by the glazing system as a whole in its installed condition. The specification therefore applies to both the glazing element and all seals on any openable part of the system. It should be confirmed with any supplier that the full glazing system supplied complies with the requirements stated in Table 7.2 and 7.2.1. Data has been used from Guardian Glass, see Appendix D for details.

7.3 ASSESSMENT OF EXISTING FAÇADE

In order to determine areas where the existing glazing could be retained, onsite measurements were taken in accordance with ISO 12354-3: 2017 'Building acoustics — Estimation of acoustic performance of buildings from the performance of elements — Part 3: Airborne sound insulation against outdoor sound' [ISO 12354-3].
Concurrent internal and external measurements were taken in order to measure the reduction of external noise through the façade to internal space. Corrections for the façade area and room properties were then added in accordance with ISO 12354-3 to calculate the apparent sound reduction index of the existing façade. The calculated apparent sound reduction index of the existing façade is shown in Table 7.3.

Calculated SRI					
Frequency, Hz/dB					$D_{,n.e}$
125	250	500	1K	2K	4k
21	22	28	30	28	29

Table 7.3 – Calculated SRI of Existing Façade

Calculations were then carried out to determine the level of internal noise in each assessment area, with the external façade as existing.

Existing rear façade glazing can be retained for all rooms. It is noted that the current glazing has no ventilation. Ventilation as stated in 9.0 will need to be added.

8.0 INTERNAL NOISE CRITERIA

Monitoring Period	Noise Criteria L_{AMAX}	No. times exceeded L_{AMAX}
07:00 – 23:00	55dB	4
23:00 – 07:00	45dB	5

Table 8.0 – Noise Criteria L_{AMAX} - (Location1 – Front Façade)

Monitoring Period	Noise Criteria L_{AMAX}	No. times exceeded L_{AMAX}
07:00 – 23:00	55dB	1
23:00 – 07:00	45dB	4

Table 8.1 - Noise Criteria L_{AMAX} - (Location 2 – Rear Façades)

Monitoring Period	Noise Criteria L_{Aeq}	Internal Noise Level
07:00 – 23:00	35dB	34dB
23:00 – 07:00	30dB	24dB

Table 8.2 - Noise Criteria L_{Aeq} - (Location1 – Front Façade)

Monitoring Period	Noise Criteria L_{Aeq}	Internal Noise Level
07:00 – 23:00	35dB	28dB
07:00 – 23:00 – Flat 2	35dB	29dB
23:00 – 07:00	30dB	24dB

Table 8.3 - Noise Criteria L_{Aeq} - (Location 2 – Rear Façades)

9.0 VENTILATION AND OVERHEATING

Guidance on ventilation and associated acoustic considerations is given in Acoustic Ventilation and Overheating – Residential Design Guide [AVO] issued jointly by the Association of Noise Consultants and the Institute of Acoustics. In this guide, the need for ventilation (as falls under the requirements of Approved Document F [ADF] are covered in three main requirements as follows:

- Whole Dwelling Ventilation - General ventilation – continuous ventilation of rooms or spaces at a relatively low rate
- Extract Ventilation - Removal of air from a space or spaces (typically stale air from bathrooms or kitchens) to outside
- Purge Ventilation - Manually controlled removal of air at a high rate to eliminate fumes and odours, e.g. during painting and decorating or from burnt food. May be provided by natural or mechanical means.

Four main template systems for providing each of the above ADF ventilation requirements are summarised in the AVO guide as shown in Table 9.0.

Ventilation System	Method Of Whole Dwelling Ventilation	Method of Extract Ventilation	Method of purge Ventilation
System 1 (Background Ventilators and intermittent extract Fans	Background ventilators (Trickle Vents)	Intermittent extract fans	Typically provided by opening windows
System 2 (Passive Stack)	Background ventilators (Trickle Vents) & Passive Stack	Continuous via passive stack	Typically provided by opening windows
System 3 (Contunuous Mechanical Extract (MEV)	Continuous mechanical extract (low rate), trickle vents provide fresh air	Continuous mechanical extract (high rate), trickle vents provide fresh air	Typically provided by opening windows
System 4 (Continuously mechanical supply and extract with heat recovery (MVHR)	Continuous mechanical supply and extract (low rate)	Continuous mechanical supply and extract (high rate)	Typically provided by opening windows

Table 9.0 – Summary of ADF Ventilation Requirements

Where possible, natural forms of ventilation are typically preferred. However, in high noise areas, it may be necessary to recommend System 4, in order to minimise penetrations through the external building façade, which weaken the overall sound reduction performance.

The Below Table outlines the appropriate ventilation strategies for this development.

Ventilation Strategy (according to ADF)	FRONT FAÇADE	REAR FAÇADE
System 1: Intermittent Extract Fans System 2: Passive Stack Ventilation	✗	✗
System 3: Continuous Mechanical Extract (MEV)	✓	✓
System 4: Continuous Mechanical Supply & Extract with Heat Recovery (MVHR)	✓	✓

Table 9.0.1 – Ventilation Options

Calculations were carried out using Titon Acoustic ventilators - V25 + C25. Details Below:

Dn,e dB					
Frequency, Hz/dB					$D_{,n.e}$
125	250	500	1K	2K	**36**
36	38	36	32	37	

Table 9.0.2 - Required ventilator performance

It should be ensured that all mechanical extract ventilation is designed to not exceed the internal noise criteria stated in Table 2.4.1.

To stairwells, no specific acoustic measures would be necessary and standard trickle vents would be appropriate.

10.0 INTERNAL SOUND INSULATION ASSESSMENT

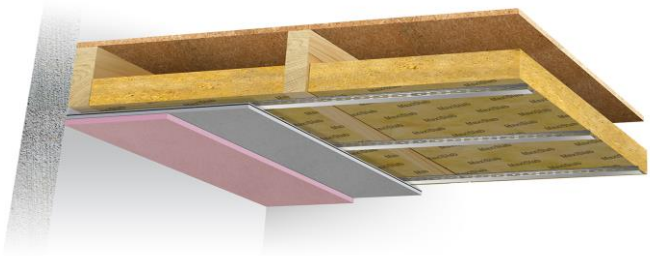
The floor and wall structure may be subject to pre-completion testing in accordance with requirements of The Building Regulations 2010 Approved Document E (2003 Edition & amendments). It should be expected that the proposed dwelling will exceed the minimum performance standards of the Regulations, as stipulated between dwellings in terms of dB DnT,w +Ctr.

10.1 PROPOSED FLOOR SYSTEM BETWEEN RESIDENTIAL UNITS

Between Joists 100mm mineral wool 45kg/m3 rigid slabs to be laid tight.

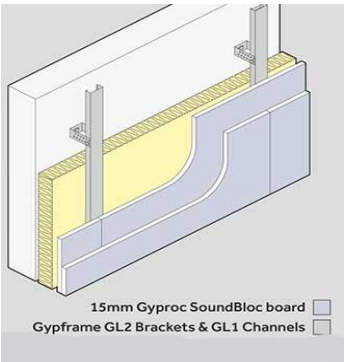
18mm T&G chipboard sub floor or original floorboards to be laid and screwed tight. 28mm T&G Deckfon chipboard or alternatively 10mm carpet underlay with tapped seems and 22mm T&G Chipboard to be laid over, creating a floating floor. A separation gap with a minimum 3mm must be left between walls and floor and then filled with acoustic sealant to prevent flanking noise.

25mm Resilient bars to be installed and fitted with 1x layer of Soundbloc Plasterboard and 1 x layer of Firestop Plasterboard with staggered joins.



10.2 PARTY WALLS

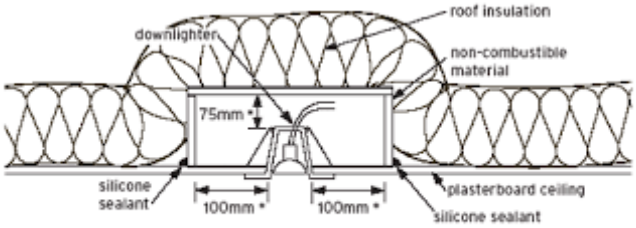
Separating walls are to be built as British Gypsum Quiet Wall, high performance acoustic wall system. Mineral wool infill to be a minimum of 50mm Rw45. (See Detail Below).



Alternatively, 75mm CLS stud wall with a 75mm cavity can be erected and secured via the ceiling joist and floor joist but not the party wall directly. The wall must sit on a 15mm strip of Soundbloc Plasterboard (Blue Board) between floor and ceiling to act as a deflection strip and minimise flanking noise. The cavity must be insulated with Rw45/50mm Mineral wool with 45kg/m3 density and left with a clear 25mm airgap. Fitting of one side of the party wall would be sufficient on solid construction.

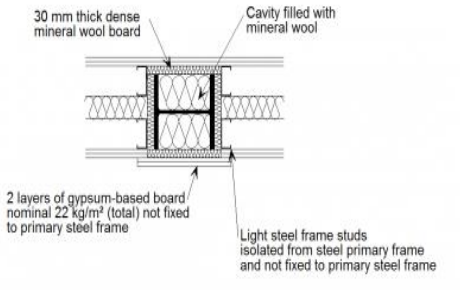
10.3 LIGHTING

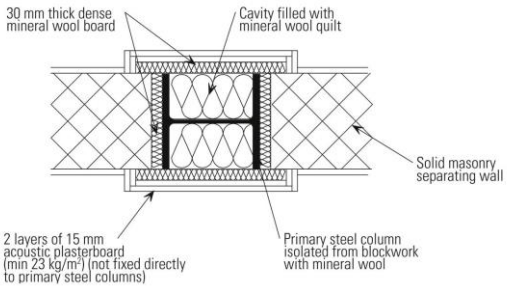
Any down lighting will be boxed with 15mm Sounbloc plasterboard and sealed with acoustic sealant from above. Alternatively, an acoustic downlight unit would be suitable.



10.4 STEEL BEAMS & WASTE PIPES

All steel beams and waste pipes should be boxed and infilled with 100mm 45kg/m3 mineral wool and encased with 15mm soundbloc plaster board, where possible a 20-25mm air gap should be incorporated.





10.5 LIGHTWEIGHT WALL DETAILING

Socket backs in lightweight partitions should be boxed in using two layers of plasterboard of the same mass as the partition wall and should be staggered by at least 300mm. Party walls should 'break' any lightweight flanking constructions to ensure acoustic discontinuity between the leaves of the partition.

10.6 WALL JUNCTIONS

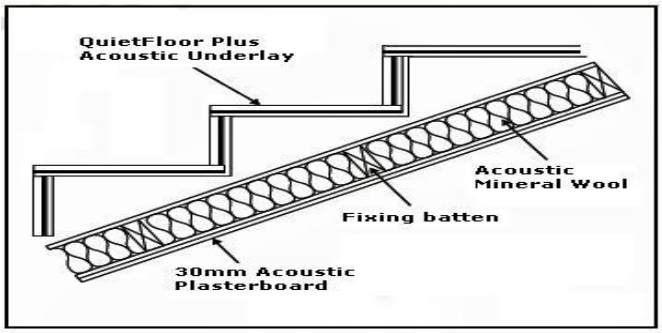
Where party walls meet other constructions, the party wall construction must 'break' the flanking construction, such as the plasterboard lining of external walls. Blockwork for internal leaves of external and flanking walls should have a minimum density of 1850kg/m3 . With these proposed works implemented the flanking construction is expected to achieve the uprated performance requirements. Cavity stops should be used at all junctions between walls and floors in the external cavity.

10.7 COMMUNAL AREAS

Soft closers are to be installed to communal and residential main doors to prevent high Reverberation Time (RT60) i.e slamming door.
Acoustic seals and drop seals to be installed to all main residential doors to prevent break in noise.

10.8 PARTY STAIRCASE

Party walls with stairs adjoining will be lined with15mm Soundbloc plasterboard.
The stair treads will have Acoustilay 8 or equivalent glued to each individual tread to prevent impact noise.



10.9 ENTRANCE DOORS

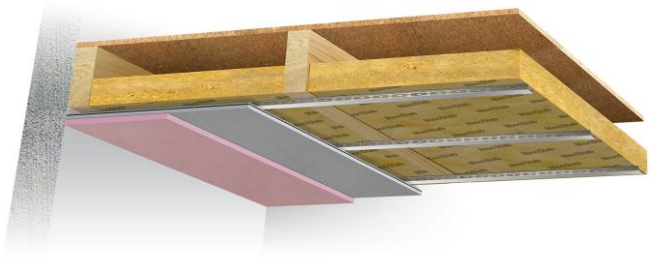
Entrance doors should have a double acoustic seal to prevent noise break in form communal hallways.

10.10 PROPOSED FLOOR SYSTEM BETWEEN COMMERCIAL AND RESIDENTIAL

Between Joists 100mm mineral wool 65kg/m3 rigid slabs to be laid tight.

18mm T&G chipboard sub floor or original floorboards to be laid and screwed tight. 28mm T&G Deckfon chipboard or alternatively 10mm carpet underlay with tapped seems and 22mm T&G Chipboard to be laid over, creating a floating floor. A separation gap with a minimum 3mm must be left between walls and floor and then filled with acoustic sealant to prevent flanking noise.

25mm Resilient bars to be installed and fitted with 1x layer of Soundbloc Plasterboard and 1 x layer of Firestop Plasterboard with staggered joins.



11.0 SUMMARY AND CONCLUSIONS

A baseline noise survey has been undertaken by DAA Group to establish the prevailing noise climate in the locality of 105-111 Winchester Road, Chandlers Ford, Hampshire SO53 2ZA in support of a Planning Application for the addition of a 2nd floor to the front elevation.

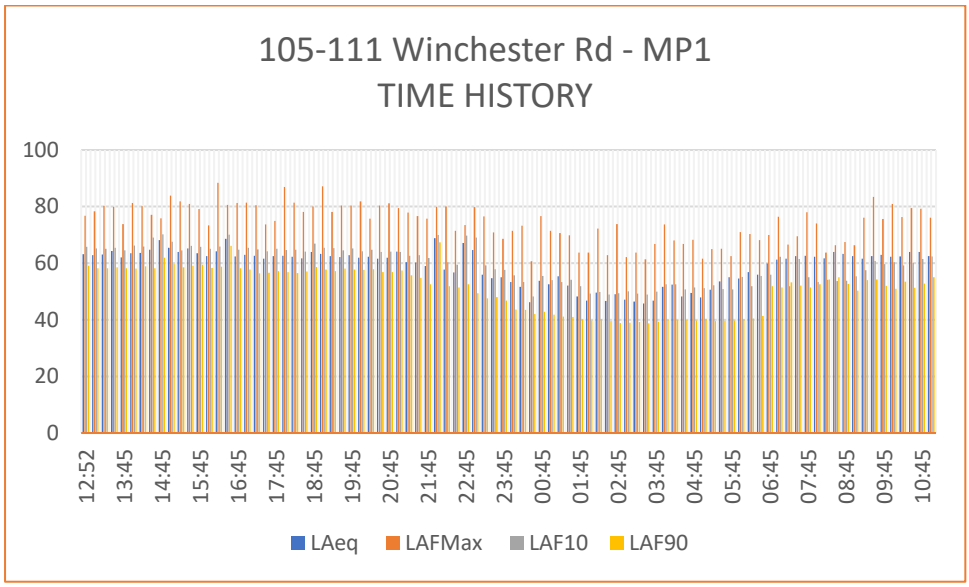
Using results of the noise survey, the sound insulation performance for the whole building envelope including glazing (windows) is assessed, and a scheme of noise mitigation measures is established and included in the report verified by BS8233:2014 rigorous method building envelope sound insulation calculations.

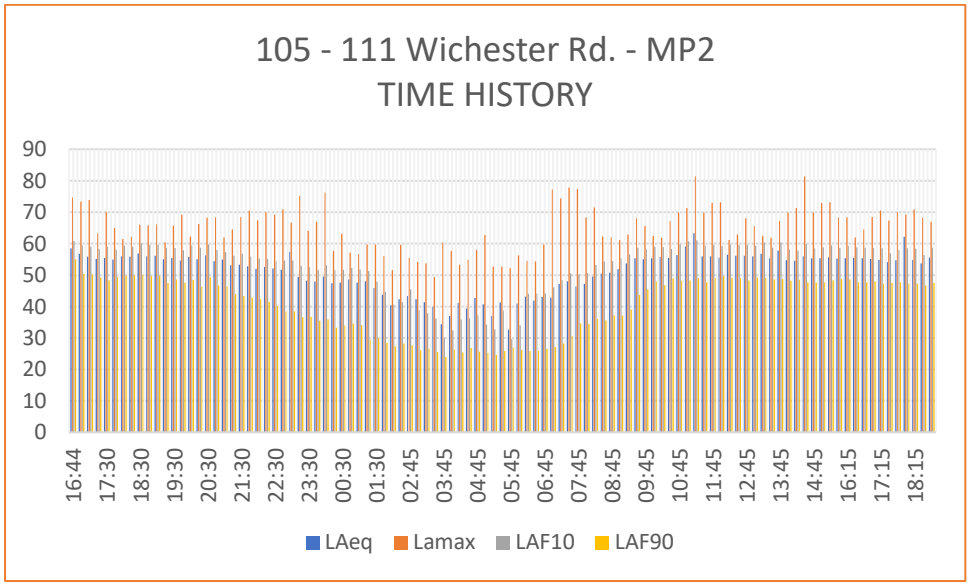
A scheme of noise mitigation measures in the report provides specification details as appropriate for sound insulation treatment to the separating floor and walls.

A BS4142:2014+A1:2019 Assessment has been carried to assess the noise from the nearby existing commercial plant.

It is concluded that, the impact of noise will not prejudice the amenities of any future occupants provided the above points are taken into consideration.

APPENDIX A – MEASUREMENTS





APPENDIX B - ACOUSTIC TERMINOLOGY

B.1 WEIGHTED DECIBEL, dB(A)

The unit generally used for measuring environmental, traffic or industrial noise is the A-weighted sound pressure level in decibels, denoted dB(A). The weighting is based on the frequency response of the human ear and has been found to correlate well with human subjective reactions to various sounds. An increase or decrease of approximately 10 dB corresponds to a subjective doubling or halving of the loudness of a noise, and a change of 2 to 3 dB is subjectively barely perceptible.

B.2 EQUIVALENT CONTINUOUS SOUND LEVEL, LAeq

Another index for assessment for overall noise exposure is the equivalent continuous sound level, L_{Aeq}. This is a notional steady level which would, over a given period, deliver the same sound energy as the actual time-varying sound over the same period.

B.3 MAXIMUM NOISE LEVEL, LAmax

The maximum noise level identified during a measurement period. Experimental data has shown that the human ear does not generally register the full loudness of transient sound events of less than 125 ms in duration.

B.4 NOISE RATING, NR

Noise ratings are used as a single figure criterion for specifying services noise in buildings. Each noise rating value has an associated spectrum of defined values in each third or octave frequency band. To determine the noise rating of a room the measured spectrum is compared to a set of noise rating curves. The highest NR curve that crosses any single frequency band of the measurement determines the noise rating for the room. The single figure noise rating is read at the 1 kHz band.

B.5 SOUND LEVEL DIFFERENCE (D)

The sound insulation required between two spaces may be determined by the sound level difference needed between them. A single figure descriptor which characterises a range of frequencies, the weighted sound level difference, D, is sometimes used (BS EN ISO 717-1). This parameter is not adjusted to reference conditions.

The standardized level difference, Dn, T is a measure of the difference in sound level between two rooms, in each frequency band, where the reverberation time in the receiving room has been normalised to 0.5 s. This parameter measures all transmission paths, including flanking paths.

The weighted standardized level difference, DnTw, is a measure of the difference in sound level between two rooms, which characterises a range of frequencies and is normalised to a reference reverberation time

B.6 SOUND REDUCTION INDEX (R)

The sound reduction index (or transmission loss) of a building element is a measure of the loss of sound through the material, i.e. its attenuation properties. It is a property of the component, unlike the sound level difference which is affected by the common area between the rooms and the acoustic of the receiving room. The weighted sound reduction index, Rw, is a single figure description of sound reduction index characterising a range of frequencies, which is defined in BS EN ISO 717-1: 1997. The Rw is calculated from measurements in an acoustic laboratory

B.7 STATISTICAL NOISE LEVELS (L_{A90}, (T) L_{A1}, (T) L_{A10}, (T) etc.)

For levels of noise that vary widely with time, for example road traffic noise, it is necessary to employ an index which allows for this variation. The L_{A10} is the level exceeded for ten per cent of the time under consideration, has historically been
adopted in the UK for the assessment of road traffic noise. The LA90 is the level exceeded for ninety per cent of the time, has been adopted to represent the background noise level. The L_{A1} the level exceeded for one per cent of the time, is representative of the maximum levels recorded during the sample period. A weighted statistical noise levels are denoted LA10, dB LA90, dB. etc. The reference time (T) is normally included, e.g. LA10, (5min), & LA90, (8hr).

B.8 TYPICAL NOISE LEVELS

Typical noise levels are given in the following table.

Noise Level dB(A)	Example
130	Threshold of pain
120	Jet aircraft take-offs at 100 m
110	Chain saw at 1 m
100	Inside disco
90	Heavy lorries at 5 m
80	Kerbside of busy street
70	Loud radio (in typical domestic room)
60	Office or restaurant
50	Domestic fan heaters at 1m
40	Living room
30	Ventilation Noise in Theatre
20	Remote countryside on still night
10	Sound insulated test chamber
0	Threshold of hearing.

APPENDIX C - CALCULATIONS

NOISE EMISSION CALCULATION														
ITEM	**PARAMETER**			**HZ**		**63**	**125**	**250**	**500**	**1K**	**2K**	**4K**	**8K**	**dBA**
1	**Schedule of Plant**	Qty												
2	**Fujitsu**													
3	AOYG09LEC	1	Spl	dB	+	49	49	47	41	39	38	34	26	43
4														
5														
6	Revised Spl:	5	Spl	dB	+	56	56	54	48	46	45	41	33	50
7														
8														
9														
10														
11	Distance to nearest receptor Metres:	6		dB	-	**-16**	**-16**	**-16**	**-16**	**-16**	**-16**	**-16**	**-16**	**-16**
12	SPL=L1-20log$_{10}$(r2/r1)	1												
13														
14	Natural Barrier		∂	dB	-	-5	-5	-5	-5	-5	-5	-5	-5	-5
15														
16	Spl at receptor			dB	+	35	35	33	27	25	24	20	12	29
17														
18														
19	Façade correction	3.0		dB	+	3	3	3	3	3	3	3	3	3
20	Intermittant noise correction	0		dB	+	0	0	0	0	0	0	0	0	0
21														
22														
23	Specific noise level at receptor			dB	+	38	38	36	30	28	27	23	15	32
24	(1m outside noise sensitive window)													
25	**Lowest Background Noise Levels:(L_{A90})**													
26	**Daytime - 07:00 - 23:00**	**49**												**49**
27	**Difference:** (Assessment level)			dB	-									**-17**
28														

NOISE EMISSION CALCULATION														
ITEM	**PARAMETER**			**HZ**		**63**	**125**	**250**	**500**	**1K**	**2K**	**4K**	**8K**	**dBA**
1	**Schedule of Plant**	Qty												
2	**Fujitsu**													
3	AOYG09LEC	1	Spl	dB	+	49	49	47	41	39	38	34	26	43
4														
5														
6	Revised Spl:	5	Spl	dB	+	56	56	54	48	46	45	41	33	50
7														
8														
9														
10														
11	Distance to nearest receptor Metres:	15		dB	-	**-24**	**-24**	**-24**	**-24**	**-24**	**-24**	**-24**	**-24**	**-24**
12	SPL=L1-20log$_{10}$(r2/r1)	1												
13														
14	Natural Barrier		∂	dB	-	-3	-3	-3	-3	-3	-3	-3	-3	-3
15														
16	Spl at receptor			dB	+	29	29	27	21	19	18	14	6	23
17														
18														
19	Façade correction	3.0		dB	+	3	3	3	3	3	3	3	3	3
20	Intermittant noise correction	0		dB	+	0	0	0	0	0	0	0	0	0
21														
22														
23	Specific noise level at receptor			dB	+	32	32	30	24	22	21	17	9	26
24	(1m outside noise sensitive window)													
25	**Lowest Background Noise Levels:(L_{A90})**													
26	**Daytime - 07:00 - 23:00**	**49**												**47**
27	**Difference:** (Assessment level)			dB	-									**-21**
28														

NOISE EMISSION CALCULATION														
ITEM	**PARAMETER**			**HZ**		**63**	**125**	**250**	**500**	**1K**	**2K**	**4K**	**8K**	**dBA**
1	**Schedule of Plant**	Qty												
2														
3	Fujitsu - AOYG36KBTA5	1	Spl	dB	+	68	66	54	51	49	44	42	37	55
	Kitchen Extraction Outlet	1	Spl	dB	+	78	76	64	61	59	54	52	47	65
4														
5														
6	Revised Spl:	1	Spl	dB	+	78	76	64	61	59	54	52	47	65
7														
8														
9														
10														
11	Distance to nearest receptor Metres:	12		dB	-	**-22**	**-22**	**-22**	**-22**	**-22**	**-22**	**-22**	**-22**	**-22**
12	$SPL=L1-20\log_{10}(r2/r1)$	1												
13														
14	Natural Barrier		∂	dB	-	5	5	5	5	5	5	5	5	5
15														
16	Spl at receptor			dB	+	51	49	37	34	32	27	25	20	38
17														
18														
19	Façade correction	3.0		dB	+	3	3	3	3	3	3	3	3	3
20	Intermittant noise correction	0		dB	+	0	0	0	0	0	0	0	0	0
21														
22														
23	Specific noise level at receptor			dB	+	54	52	40	37	35	30	28	23	41
24	(1m outside noise sensitive window)													
25	**Lowest Background Noise Levels:(L_{A90})**													
26	**Day Time (07:00-23:00)**													**47**
27	**Difference:** (Assessment level)			dB	-									**-6**
28														

Calculation Sheet

MP1 - 07:00 - 23:00 to LR

		Octave Band Centre Frequency (Hz)								
		63	125	250	500	1k	2k	4k	8k	
Noise Source										
Noise Source - MP1 - 07:00 - 23:00										
Noise Levels		**66.0**	**66.0**	**60.0**	**59.0**	**57.0**	**52.0**	**44.0**	**44.0**	**61.4 dBA**
Composite SRI										
Facade Width (m)	4.0									
Facade Height (m)	3.0									
Main Element - External Wall										
SRI		-	41	43	48	50	55	55	-	Rw 51
Window Width (m)	0.5									
Window Height (m)	1.0									
No. of Windows (no)	3.0									
Glazed Element - 34Rw										
SRI		-	28	24	29	41	37	31	-	Rw 34
No. of Vents (no)	3.0									
Vent - Standard Vents										
Dne		36	36	38	36	32	37	39	48	Dnew 36
		-	*-30.5*	*-30.3*	*-31.0*	*-28.0*	*-32.8*	*-33.8*	-	
10 log (S/A)										
Internal Receiver - LR										
		-	*-1.1*	*-1.1*	*-1.1*	*-1.1*	*-1.1*	*-1.1*	-	
+3										
		-	*3.0*	*3.0*	*3.0*	*3.0*	*3.0*	*3.0*	-	
Internal Receiver Noise										
Internal Receiver Noise - LR										
Reverberant Field, LPrev		-	**37.4**	**31.6**	**29.9**	**30.9**	**21.1**	**12.1**	-	**33.5 dBA**

Calculation Sheet

MP1 23:00 - 07:00 to BR

		Octave Band Centre Frequency (Hz)								
		63	125	250	500	1k	2k	4k	8k	
Noise Source										
Noise Source - MP1 23:00 - 07:00										
Noise Levels		**55.0**	**55.0**	**49.0**	**48.0**	**46.0**	**41.0**	**33.0**	**33.0**	**50.4 dBA**
Composite SRI										
Facade Width (m)	3.0									
Facade Height (m)	3.0									
Main Element - External Wall										
SRI		-	41	43	48	50	55	55	-	Rw 51
Window Width (m)	0.5									
Window Height (m)	1.0									
No. of Windows (no)	3.0									
Glazed Element - 34Rw										
SRI		-	28	24	29	41	37	31	-	Rw 34
No. of Vents (no)	3.0									
Vent - Standard Vents										
Dne		36	36	38	36	32	37	39	48	Dnew 36
		-	*-29.3*	*-29.1*	*-29.7*	*-26.7*	*-31.5*	*-32.6*	-	
10 log (S/A)										
Internal Receiver - BR										
		-	*-1.1*	*-1.1*	*-1.1*	*-1.1*	*-1.1*	*-1.1*	-	
+3										
		-	*3.0*	*3.0*	*3.0*	*3.0*	*3.0*	*3.0*	-	
Internal Receiver Noise										
Internal Receiver Noise - BR										
Reverberant Field, LPrev		-	**27.6**	**21.8**	**20.2**	**21.2**	**11.4**	**2.3**	-	**23.7 dBA**

Calculation Sheet

MP1 - 07:00 - 23:00 to BR

		Octave Band Centre Frequency (Hz)								
		63	125	250	500	1k	2k	4k	8k	
Noise Source										
Noise Source - MP1 - 07:00 - 23:00										
Noise Levels		**66.0**	**66.0**	**60.0**	**59.0**	**57.0**	**52.0**	**44.0**	**44.0**	**61.4 dBA**
Composite SRI										
Facade Width (m)	3.0									
Facade Height (m)	3.0									
Main Element - External Wall										
SRI		-	41	43	48	50	55	55	-	Rw 51
Window Width (m)	0.5									
Window Height (m)	1.0									
No. of Windows (no)	3.0									
Glazed Element - 34Rw										
SRI		-	28	24	29	41	37	31	-	Rw 34
No. of Vents (no)	3.0									
Vent - Standard Vents										
Dne		36	36	38	36	32	37	39	48	Dnew 36
		-	*-29.3*	*-29.1*	*-29.7*	*-26.7*	*-31.5*	*-32.6*	-	
10 log (S/A)										
Internal Receiver - BR										
		-	*-1.1*	*-1.1*	*-1.1*	*-1.1*	*-1.1*	*-1.1*	-	
+3										
		-	*3.0*	*3.0*	*3.0*	*3.0*	*3.0*	*3.0*	-	
Internal Receiver Noise										
Internal Receiver Noise - BR										
Reverberant Field, LPrev		-	**38.6**	**32.8**	**31.2**	**32.2**	**22.4**	**13.3**	-	**34.7 dBA**

Calculation Sheet

MP2 07:00 - 23:00 to LR

		Octave Band Centre Frequency (Hz)								
		63	125	250	500	1k	2k	4k	8k	
Noise Source										
Noise Source - MP2 07:00 - 23:00										
Noise Levels		**72.0**	**65.0**	**59.0**	**58.0**	**56.0**	**51.0**	**43.0**	**43.0**	**60.5 dBA**
Composite SRI										
Facade Width (m)	4.0									
Facade Height (m)	3.0									
Main Element - External Wall										
SRI		42.0	41.0	43.0	48.0	50.0	55.0	55.0	56.0	Rw 51
Window Width (m)	1.0									
Window Height (m)	2.0									
No. of Windows (no)	3.0									
Glazed Element - 34Rw										
SRI		34.0	28.0	24.0	29.0	41.0	37.0	31.0	38.0	Rw 34
		-36.37	*-30.80*	*-26.96*	*-31.96*	*-43.50*	*-39.94*	*-33.99*	*-40.94*	
10 log (S/A)										
Internal Receiver - LR										
		-1.1	*-1.1*	*-1.1*	*-1.1*	*-1.1*	*-1.1*	*-1.1*	*-1.1*	
+3										
		3.0	*3.0*	*3.0*	*3.0*	*3.0*	*3.0*	*3.0*	*3.0*	
Internal Receiver Noise										
Internal Receiver Noise - LR										
Reverberant Field, LPrev		**37.5**	**36.1**	**33.9**	**27.9**	**14.4**	**13.0**	**10.9**	**4.0**	**29.2 dBA**

Calculation Sheet

MP2 23:00 - 07:00 to BR

		Octave Band Centre Frequency (Hz)								
		63	125	250	500	1k	2k	4k	8k	
Noise Source										
Noise Source - MP2 23:00 - 07:00										
Noise Levels		**56.0**	**54.0**	**48.0**	**47.0**	**45.0**	**40.0**	**32.0**	**32.0**	**49.4 dBA**
Composite SRI										
Facade Width (m)	3.0									
Facade Height (m)	3.0									
Main Element - External Wall										
SRI		-	41	43	48	50	55	55	-	Rw 51
Window Width (m)	1.0									
Window Height (m)	2.0									
No. of Windows (no)	1.0									
Glazed Element - 29Rw										
SRI		-	14	19	24	31	41	21	-	Rw 29
No. of Vents (no)	1.0									
Vent - Standard Vents										
Dne		36	36	38	36	32	37	39	48	Dnew 36
		-	*-20.4*	*-25.2*	*-29.3*	*-30.5*	*-36.2*	*-27.2*	-	
10 log (S/A)										
Internal Receiver - BR										
		-	*-1.1*	*-1.1*	*-1.1*	*-1.1*	*-1.1*	*-1.1*	-	
+3										
		-	*3.0*	*3.0*	*3.0*	*3.0*	*3.0*	*3.0*	-	
Internal Receiver Noise										
Internal Receiver Noise - BR										
Reverberant Field, LPrev		**-**	**35.5**	**24.7**	**19.6**	**16.4**	**5.7**	**6.7**	**-**	**23.5 dBA**

Calculation Sheet

MP2 LAMAX to BR

		Octave Band Centre Frequency (Hz)								
		63	125	250	500	1k	2k	4k	8k	
Noise Source										
Noise Source - MP2 LAMAX										
Noise Levels		**65.0**	**63.0**	**57.0**	**56.0**	**54.0**	**49.0**	**41.0**	**41.0**	**58.4 dBA**
Composite SRI										
Facade Width (m)	3.0									
Facade Height (m)	3.0									
Main Element - External Wall										
SRI		-	41	43	48	50	55	55	-	Rw 51
Window Width (m)	1.0									
Window Height (m)	2.0									
No. of Windows (no)	1.0									
Glazed Element - 29Rw										
SRI		-	14	19	24	31	41	21	-	Rw 29
No. of Vents (no)	1.0									
Vent - Standard Vents										
Dne		36	36	38	36	32	37	39	48	Dnew 36
		-	*-20.4*	*-25.2*	*-29.3*	*-30.5*	*-36.2*	*-27.2*	-	
10 log (S/A)										
Internal Receiver - BR										
		-	*-1.1*	*-1.1*	*-1.1*	*-1.1*	*-1.1*	*-1.1*	-	
+3										
		-	*3.0*	*3.0*	*3.0*	*3.0*	*3.0*	*3.0*	-	
Internal Receiver Noise										
Internal Receiver Noise - BR										
Reverberant Field, LPrev		**-**	**44.5**	**33.7**	**28.6**	**25.4**	**14.7**	**15.7**	**-**	**32.5 dBA**

Acoustic Performance

Glazing Configuration

3mm Float Glass

10mm Cavity

3mm Float Glass

.

Sound Reduction Indices

Frequency, Hz / dB						Rw	C	Ctr	OITC	STC
125	250	500	1000	2000	4000	29	-1	-4	23	28
14	19	24	31	41	21					

Disclaimer: The acoustic performance data provided in the reports is based on a test protocol or an estimation and may be used if user actual glazing is identical to input data described herein. Acoustic performance data herein is only applicable for glazing dimensions 1,23 m x 1,48 m (as per testing standard). Estimation of acoustic performance is based on component-similarity assumptions which are derived from measured data and interpolation to expand the database of values from test protocols. Due to inherent variations in acoustic performance when testing in accordance with EN ISO 10140-3/EN ISO 10140-2, some variation in the calculated performance can also be expected. As such, the weighted performance, Rw, and adaptation terms, C and Ctr, should typically be considered to be accurate within ±2 dB. However, wider deviations can occur. Actual performance may vary according to the glazing dimensions, frame system, noise sources and many other parameters. The acoustic performance data herein should not be used as a substitute for tests of actual glazing. For more information please consult Assumptions and Terminology section in Guardian Acoustic Assistant. <P>By accessing this calculator, you agree not to alter or modify the generated report data and information, by any means. Any manual alteration will be your own responsibility and will annul all the content of the report.<P>

Tuesday, June 27, 2023 | Acoustic database 20210629

Acoustic Performance

Glazing Configuration

5mm Float Glass

14mm Cavity

6mm Float Glass

.

Sound Reduction Indices

Frequency, Hz / dB						Rw	C	Ctr	OITC	STC
125	250	500	1000	2000	4000	34	-1	-4	29	34
28	24	29	41	37	31					

Disclaimer: The acoustic performance data provided in the reports is based on a test protocol or an estimation and may be used if user actual glazing is identical to input data described herein. Acoustic performance data herein is only applicable for glazing dimensions 1,23 m x 1,48 m (as per testing standard). Estimation of acoustic performance is based on component-similarity assumptions which are derived from measured data and interpolation to expand the database of values from test protocols. Due to inherent variations in acoustic performance when testing in accordance with EN ISO 10140-3/EN ISO 10140-2, some variation in the calculated performance can also be expected. As such, the weighted performance, Rw, and adaptation terms, C and Ctr, should typically be considered to be accurate within ±2 dB. However, wider deviations can occur. Actual performance may vary according to the glazing dimensions, frame system, noise sources and many other parameters. The acoustic performance data herein should not be used as a substitute for tests of actual glazing. For more information please consult Assumptions and Terminology section in Guardian Acoustic Assistant. <P>By accessing this calculator, you agree not to alter or modify the generated report data and information, by any means. Any manual alteration will be your own responsibility and will annul all the content of the report.<P>

Tuesday, June 27, 2023 | Acoustic database 20210629 | Protocol №: 08/32310357 assumption, dated , according to

Primary Glass Thickness	Secondary Glass Thickness	Rw dB values for Selectaglaze Ltd Secondary Glazing Systems*																	
		S10	S20 VS	S30	S40 SHC	S40 DSH	S40 FL	S45 SHC	S45 DSH	S45 FL	S46 FL	S50 SHC	S50 FL	S55	S60TV S	S80	S85 SH	S90 VS	S95VS
		100mm cavity																	
6 mm	4mm toughened glass	43	43	42	45	43	45	45	43	45					44				
6 mm	4mm float glass	43	43	42	45	43	45	45	43	45					44				
6 mm	6mm	43	43	42	45	43	45	45	43	45	45	44	45		44	44		44	
6 mm	6.4mm	43	43	42	45	43	45	45	43	45					44	44		44	
6 mm	6.4mmSS	44	44	43	46	44	46	46	44	46					45	45		45	
6 mm	6.8mm	44	44	43	46	44	46	46	44	46					45	45		45	
6 mm	6.8mmSS	44	44	43	46	44	46	46	44	46					45	45		45	
6 mm	7.5mm				46	44	46					45	46	44		45		44	44
6 mm	8mm float	45	45	44	47	45	47	47	45	47					46	46		46	
6 mm	8.8mm				47	45	47									46		46	
6 mm	8.8mmSS				47	45	47					46				46		46	
6 mm	9.5mm				47	45	47				47	46	47	45		46	45	46	45
6 mm	10mm				47	45	47									46		46	
6 mm	10.8mmSS				48	46	48					47				47		46	
6 mm	10.8mm				48	46	48					47				47		46	
6 mm	11.5mm				48	46	48				48	47	48	46		47	46	47	46
6 mm	12mm				48	46	48									47		46	

Rw Correction Factors (based upon laboratory tested scenarios)

acoustic tiles on 3No. Sides - low spec glass	+2 dB
acoustic tiles on 3No. Sides - high spec glass	+1 dB
acoustic vent 4000 open	-2 dB
trickle vent 4000 open	-3 dB
trickle vent 8000 open	-5 dB

Values have been interpolated and extrapolated from Rw values achieved at Taylor Woodrow on 21 to 22 March 2006

100mm Cavity

* See attached Selectaglaze drawings in Appendix A illustrating secondary glazing systems listed above