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STRUCTURAL ENGINEERING CALCULATIONS,
FOR NEW DWELLING AT BIRCHWOOD GARDENS,
HEDGE END, SOUTHAMPTON.

CLIENT: GLEN CRUMP

DESIGNED TO THE FOLLOWING CODES:
EC0, EC1 (ACTIONS ON STRUCTURES)
EC2 (CONCRETE)
EC3 (STEEL)
EC5 (TIMBER)
EC6 (MASONRY)

DESCRIPTION OF WORKS

The client proposes to build a new dwelling close to existing mature trees. The proposal is to construct the house on a piled raft foundation which would be supported on helical screw piles to avoid damage to the roots and compaction of the ground around the trees.

The formwork for the raft will be Dufaylite clayboard which is a collapsible, biodegradable formwork which is washed through to weaken it after the slab has reached sufficient strength. Over time this then degrades naturally allowing water and oxygen to reach the roots below the tree without causing any compaction or permanent damage to the trees root system.

At or before construction, the buttress roots of the tree will need to be mapped out (with localized trial holes) to ensure that the new pile positions do not clash with these and cause to damage to them.

Job Name: Birchwood, Hedge End				
Job Number: 240913	Date:	14/12/2025	By:	AD
GENERAL LOADINGS	SLS LOADS		ULS LOADS	
1. Trussed Roof (30°)	Dead (kN/m ²)	Live (kN/m ²)	Dead (kN/m ²)	Live (kN/m ²)
Trussed Rafters	0.07			
Clay Tiles	0.65			
Felt and Battens	0.03			
Snow Load/ maintenance		0.75		
Slope load	0.75			
Roof Pitch	30			
Plan load	0.87			
Trussed Ceiling Joists	0.08			
Insulation	0.05			
12.5mm Plasterboard + skim	0.15			
18mm Chipboard	0.18			
Storage		0.25		
Total Dead	1.33		1.79	
Total Live		1.00		1.5
Total Dead and Live	2.33		3.29	
2. External Wall	Dead (kN/m ²)		Dead (kN/m ²)	
Lightweight block 100mm	1.00			
Insulation	0.05			
12.5mm Plasterboard + skim	0.15			
Brick outer leaf	2.10			
Total Dead	3.30		4.455	
3. Ground Floor	Dead (kN/m ²)	Live (kN/m ²)	Dead (kN/m ²)	Live (kN/m ²)
200mm suspended slab	4.80			
75mm Screed	1.65			
Insulation	0.05			
Internal Partitions	0.50			
Domestic Load		1.50		
Total Dead	7.00		9.45	
Total Live		1.50		2.25
Total Dead and Live	8.50		11.70	

AD Civil & Structural Engineers

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Loadings

1) Slab internal loading = $7.0 \text{ DL} + 1.50 \text{ UL} = 8.50 \text{ kN/m}^2$. (ULS = 11.70 kN/m^2)

2) Front wall loading = Truss $\times \frac{6.9}{2} + 0.3 \text{ m} = 4.99 \text{ DL}$; 3.75 UL
Wall $\times 2.5 = 8.25 \text{ DL}$

total load = 13.24 DL (kN/m) SLS load = 16.99 kN/m
 3.75 UL (kN/m) ULS load = 23.5 kN/m

3) Side wall loading = Truss $\times \frac{1.8}{2} + 0.3 \text{ m} = 1.60 \text{ kN/m DL}$; 1.20 UL
Wall $\times 2.5 = 8.25 \text{ DL}$

total load = 9.85 DL (kN/m) SLS load = 13.6 kN/m
 3.75 UL (kN/m) ULS load = $18.9 - 11$

Pile Loads

Assumed pile capacity = 73 kN SLS (for 2.0 handheld install)
= 180 kN ULS

1) Internal piles: * Based on 76R screw piles.

loaded Area = $3.2 \times 2.4 = 7.68 \text{ m}^2$

SLS load = $7.68 \times 8.50 = 65.3 \text{ kN} < 73 \therefore \text{ok.}$

ULS load = $7.68 \times 11.70 = 89.9 \text{ kN} < 180 \therefore \text{ok.}$

2) Edge Piles (Front wall):

loaded Area = $3.2 \times \left(\frac{2.4}{2} + 0.25 \right) = 4.64 \text{ m}^2$

length of wall = 3.2 m .

SLS load = $(4.64 \times 8.50) + (3.2 \times 16.99) = 93.8 \text{ kN} > 73 \therefore \text{not ok.}$

Therefore reduce spacing to 2.55 m .

New loaded area = $2.55 \times \left(\frac{2.4}{2} + 0.25 \right) = 3.7 \text{ m}^2$

new length of wall = 2.55 m .

SLS load = $(3.7 \times 8.50) + (2.55 \times 16.99) = 74.8 \text{ kN} \rightarrow \text{By inspection ok.}$

ULS load = $(3.7 \times 11.7) + (2.55 \times 23.5) = 103.2 \text{ kN} < 180 \therefore \text{ok.}$

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3) Edge piles (side wall):

$$\text{Loaded Area} = 2.4 \times \left(\frac{3.2}{2} + 0.25 \right) = 4.44 \text{ m}^2$$

$$\text{Loaded wall length} = 2.4 \text{ m}$$

$$\text{SLS Load} = (4.44 \times 8.5) + (2.4 \times 13.6) = 70.4 \text{ kN} < 73 \therefore \text{ok.}$$

$$\text{ULS Load} = (4.44 \times 11.7) + (2.4 \times 18.9) = 97.3 \text{ kN} < 180 \therefore \text{ok.}$$

4) Corner piles:

$$\text{Loaded Area} = \left(\frac{2.4}{2} + 0.25 \right) \times \left(\frac{2.55}{2} + 0.25 \right) = 2.21 \text{ m}^2$$

$$\text{Wall length} = \frac{2.4 \text{ m}}{2} \text{ (Side)} + \frac{2.55 \text{ m}}{2} \text{ (Front)}$$

$$\text{SLS Load} = (2.21 \times 8.5) + \left(\frac{2.4}{2} \times 13.6 \right) + \left(\frac{2.55}{2} \times 16.99 \right) = 56 \text{ kN} < 73 \therefore \text{ok.}$$

$$\text{ULS Load} = (2.21 \times 13.7) + \left(\frac{2.4}{2} \times 18.9 \right) + \left(\frac{2.55}{2} \times 23.5 \right) = 83 \text{ kN} < 180 \therefore \text{ok.}$$

Slab design:

$$\text{Max internal moment} = 21.2 \text{ kNm. (Sagging)}$$

$$d = 200 - 35 - 10 = 155 \text{ mm} \quad M/bd^2 f_{ck} = 0.028 \therefore z = 0.95d$$

$$A_s = \frac{M}{0.87 f_{yk} z} = \frac{21.2 \times 10^6}{0.87 \times 0.95 \times 155 \times 500} = 331 \text{ mm}^2$$

$$A_{s \min} = 0.13/100 \times 1000 \times 200 = 260 \text{ mm}^2 \therefore \text{provide } A_{s \min} \text{ mesh bottom.}$$

At edge piles provide additional H12-200 (for moment + punching)

and at corner piles provide add'l H20-200 (for punching).

over internal piles provide additional H10-200 (for ^{sagging} moment).

Project

Client

Location

Birchwood Gardens, Hedge End
Glen Crump
New Dwelling E-W

from grids

mpa

The Concrete Centre

AtoD

FLAT SLAB ANALYSIS & DESIGN to EN 1992-1 : 2004

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The Concrete Centre

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240510

MATERIALS

fck

fyk

fywk

$\Phi_{(t-t0)}$

Steel class

32

500

500

2

B

N/mm²

N/mm²

N/mm²

dg

ys

yc

Wk

20

1.15

1.50

0.3

mm

steel

concrete

mm top

0.3

mm btm

COVERS

mm

TO LAYER

Top cover

Btm cover

35

35

1

1

$\Delta_{c,dev}$

10

mm

SPANS

L (m)

SPAN 1

SPAN 2

SPAN 3

SPAN 4

SPAN 5

SPAN 6

3.190

3.190

3.190

3.190

GEOMETRY

Bay type

Slab depth, h

Int Panel width, b

INTERNAL

200

2412

mm

mm

End distance

End distance

275

275

from supt 1

from supt 5

PERIMETER LOADS

characteristic

13.60

kN/m outside supports 1 & 5

LOADING PATTERN

min

max

DEAD

IMPOSED

1.35

1.35

1.50

BS EN 1990: (6.10)

SUPPORTS

ABOVE (m)

H (mm)

B (mm)

End Cond

BELOW (m)

H (mm)

B (mm)

End Cond

Support 1

Support 2

Support 3

Support 4

Support 5

Support 6

Support 7

Usage: Vehicle<= 30kN With brittle partitions

LOADING

UDLs (kN/m²)

PLs (kN/m)

Position (m)

Dead Load

Imposed Load

Position from left

Loaded Length

Span 1

UDL

PL 1

PL 2

Part UDL

8.50

1.50

~~~~~

~~~~~

Span 2

UDL

PL 1

PL 2

Part UDL

8.50

1.50

~~~~~

~~~~~

Span 3

UDL

PL 1

PL 2

Part UDL

8.50

1.50

~~~~~

~~~~~

Span 4

UDL

PL 1

PL 2

Part UDL

8.50

1.50

~~~~~

~~~~~

Span 5

UDL

PL 1

PL 2

Part UDL

Span 6

UDL

PL 1

PL 2

Part UDL

LOADING DIAGRAM

Project Birchwood Gardens, Hedge End

Client Glen Crump

Location New Dwelling E-W, from grids A to D

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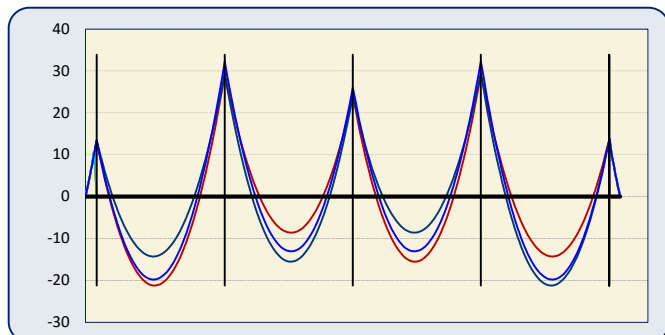


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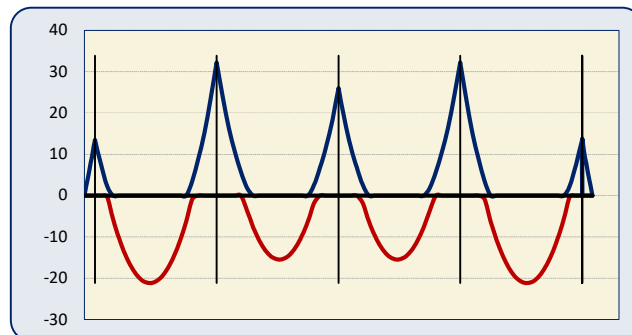
The Concrete Centre

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BENDING MOMENT DIAGRAMS (kNm)



Elastic Moments



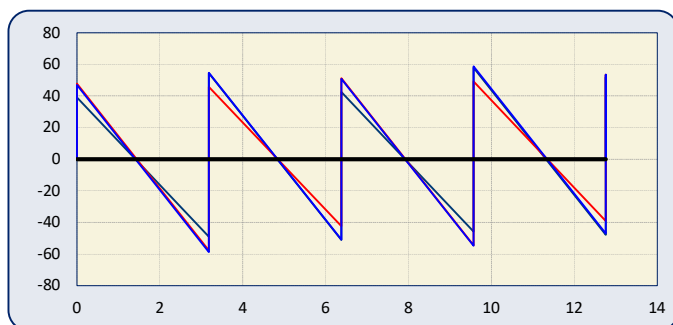
Redistributed Envelope

SUPPORT No	1	2	3	4	5		
Elastic M	13.5	32.2	26.0	32.2	13.5	~	~
Redistributed M	13.5	32.2	26.0	32.2	13.5	~	~
δ	1.000	1.000	1.000	1.000	1.000	~	~
Redistribution							
End support reinf. $\varnothing$ mm	10				10		

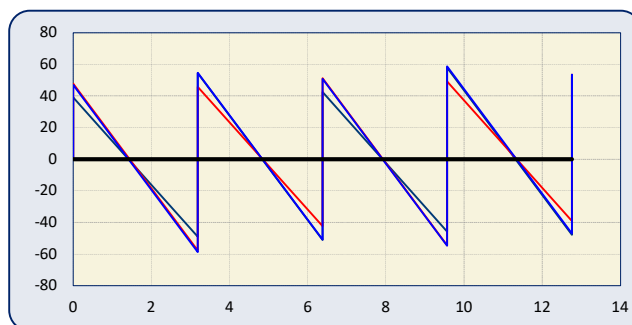
SPAN No

	1	2	3	4		
Elastic M	21.2	15.5	15.5	21.2	~	~
Redistributed M	21.2	15.5	15.5	21.2	~	~
δ	1.000	1.000	1.000	1.000	~	~

SHEAR FORCE DIAGRAMS (kN/m)



Elastic Shears



Redistributed Shears

SPAN No	1	2	3		
Elastic V	47.8	58.7	54.8	51.1	51.1 54.8
Redistributed V	47.8	58.7	54.8	51.1	51.1 54.8

SPAN No	4		
Elastic V	58.7	47.8	~ ~
Redistributed V	58.7	47.8	~ ~

REACTIONS (kN/m)

SUPPORT	1	2	3	4	5
ALL SPANS LOADED	100.3	113.5	101.7	113.5	100.3
MAXIMUM	100.3	113.5	101.7	113.5	100.3
Characteristic Dead	68.1	69.5	63.4	69.5	68.1
Characteristic Imposed	5.6	13.1	10.8	13.1	5.6
For punching	ex /by	0.0002	0.0001	0.0002	
u_1/u_1^*	1.5028				1.5028

(6.43)

(6.44)

COLUMN MOMENTS (kNm)

		1	2	3	4	5
ALL SPANS	Above					
LOADED	Below	0.0	0.0		0.0	0.0
WITH MAX	Above					
REACTION	Below	0.0	0.0		0.0	0.0

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SPAN 1			LEFT	CENTRE	RIGHT
ACTIONS	δ		1.000	1.000	1.000
	Be		365		1206
	Total M	kNm	12.3	21.2	30.6
	Mt max	kNm	50.8		165.9
MIDDLE STRIP	Width	mm	2047	1206	1206
	M	kNm	11.4	9.5	7.7
	d	mm	160.0	160.0	160.0
	As	mm²/m	84	120	96
	As deflection	mm²/m		0	
	As prov	mm²/m	262	262	262
	Top steel			Provide B10 @ 300 T1	
	Deflection		L/d = 3,190 /160 = 19.94 < 40K = 48.00		OK
COLUMN STRIP	Width	mm	365	1206	1206
	M	kNm	12.3	11.7	23.0
	d	mm	160.0	160.0	159.0
	As	mm²/m	509	146	290
	As deflection	mm²/m		0	
	As prov	mm²/m	524	262	308
	Top steel			Provide B10 @ 300 T1	
	Deflection		L/d = 3,190 /160 = 19.94 < 40K = 48.00		OK
CHECKS	% As		ok	ok	ok
	Singly reinforced		ok	ok	ok
	σs		ok	ok	ok
	max S		ok	ok	ok

SPAN 2			LEFT	CENTRE	RIGHT
ACTIONS	δ		1.000	1.000	1.000
	Be		1206		1206
	Total M	kNm	30.6	15.5	24.5
	Mt max	kNm	165.9		168.0
MIDDLE STRIP	Width	mm	1206	1206	1206
	M	kNm	7.7	7.0	6.1
	d	mm	160.0	160.0	160.0
	As	mm²/m	96	88	77
	As deflection	mm²/m		5	
	As prov	mm²/m	262	262	262
	Top steel			Provide B10 @ 300 T1	
	Deflection		L/d = 3,190 /160 = 19.94 < 40K = 48.00		OK
COLUMN STRIP	Width	mm	1206	1206	1206
	M	kNm	23.0	8.5	18.4
	d	mm	159.0	160.0	160.0
	As	mm²/m	290	107	230
	As deflection	mm²/m		8	
	As prov	mm²/m	308	262	262
	Top steel			Provide B10 @ 300 T1	
	Deflection		L/d = 3,190 /160 = 19.94 < 40K = 48.00		OK
CHECKS	% As		ok	ok	ok
	Singly reinforced		ok	ok	ok
	σs		ok	ok	ok
	max S		ok	ok	ok

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SPAN 3			LEFT	CENTRE	RIGHT
ACTIONS	δ		1.000	1.000	1.000
	Be		1206		1206
	Total M	kNm	24.5	15.5	30.6
	Mt max	kNm	168.0		165.9
MIDDLE STRIP	Width	mm	1206	1206	1206
	M	kNm	6.1	7.0	7.7
	d	mm	160.0	160.0	160.0
	As	mm ² /m	77	88	96
	As deflection	mm ² /m		5	
	As prov	mm ² /m	Provide B10 @ 300 T1 262	Provide B10 @ 300 B1 262	Provide B10 @ 300 T1 262
	Top steel			Provide B10 @ 300 T1	
	Deflection		L/d = 3,190 /160 = 19.94 < 40K = 48.00		OK
COLUMN STRIP	Width	mm	1206	1206	1206
	M	kNm	18.4	8.5	23.0
	d	mm	160.0	160.0	159.0
	As	mm ² /m	230	107	290
	As deflection	mm ² /m		8	
	As prov	mm ² /m	Provide B10 @ 225:450 T1 262	Provide B10 @ 300 B1 262	Provide B12 @ 275:550 T1 308
	Top steel			Provide B10 @ 300 T1	
	Deflection		L/d = 3,190 /160 = 19.94 < 40K = 48.00		OK
CHECKS	% As		ok	ok	ok
	Singly reinforced		ok	ok	ok
	σs		ok	ok	ok
	max S		ok	ok	ok

SPAN 4			LEFT	CENTRE	RIGHT
ACTIONS	δ		1.000	1.000	1.000
	Be		1206		365
	Total M	kNm	30.6	21.2	12.3
	Mt max	kNm	165.9		50.8
MIDDLE STRIP	Width	mm	1206	1206	2047
	M	kNm	7.7	9.5	4.7
	d	mm	160.0	160.0	160.0
	As	mm ² /m	96	120	35
	As deflection	mm ² /m		10	
	As prov	mm ² /m	Provide B10 @ 300 T1 262	Provide B10 @ 300 B1 262	Provide B10 @ 300 T1 262
	Top steel			Provide B10 @ 300 T1	
	Deflection		L/d = 3,190 /160 = 19.94 < 40K = 48.00		OK
COLUMN STRIP	Width	mm	1206	1206	365
	M	kNm	23.0	11.7	12.3
	d	mm	159.0	160.0	160.0
	As	mm ² /m	290	146	509
	As deflection	mm ² /m		15	
	As prov	mm ² /m	Provide B12 @ 275:550 T1 308	Provide B10 @ 300 B1 262	Provide B10 @ 150 T1 524
	Top steel			Provide B10 @ 300 T1	
	Deflection		L/d = 3,190 /160 = 19.94 < 40K = 48.00		OK
CHECKS	% As		ok	ok	ok
	Singly reinforced		ok	ok	ok
	σs		ok	ok	ok
	max S		ok	ok	ok

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No								
WEIGHT of REINFORCEMENT		Mid Strip	Col Strip	Type	Dia	Length	Unit wt	Weight
TOP STEEL	Support 1	7		T	10	1500	0.617	6.5
			4	T	10	1500	0.617	3.7
	Span 1	5		T	10	2725	0.617	8.4
			5	T	10	2725	0.617	8.4
	Support 2	5		T	10	1600	0.617	4.9
			4	T	12	1600	0.888	5.7
	Span 2	5		T	10	2725	0.617	8.4
			5	T	10	2725	0.617	8.4
	Support 3	5		T	10	1600	0.617	4.9
			5	T	10	1600	0.617	4.9
	Span 3	5		T	10	2725	0.617	8.4
			5	T	10	2725	0.617	8.4
	Support 4	5		T	10	1600	0.617	4.9
			4	T	12	1600	0.888	5.7
	Span 4	5		T	10	2725	0.617	8.4
			5	T	10	2725	0.617	8.4
	Support 5	7		T	10	1500	0.617	6.5
			4	T	10	1500	0.617	3.7
BTM STEEL	Span 1	5		T	10	3075	0.617	9.5
			5	T	10	3575	0.617	11.0
	Span 2	5		T	10	2950	0.617	9.1
			5	T	10	3350	0.617	10.3
	Span 3	5		T	10	2950	0.617	9.1
			5	T	10	3350	0.617	10.3
	Span 4	5		T	10	3075	0.617	9.5
			5	T	10	3575	0.617	11.0
SUMMARY Rebar for single direction only. All figures approximate - see User Guide.								
TOTAL REINFORCEMENT IN BAY (kg)				198	REINFORCEMENT DENSITY (kg/m³)			30.9

Project

Client

Location

Birchwood, Hedge End

Glen Crump

Typical Internal Pile

The Concrete Centre

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Project

Client

Location

Advisory Group

ECBP Typical Floor Column B3

PUNCHING SHEAR to BS EN 1992-1: 2004

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Project

Client

Location

PUNCHING SHEAR to BS EN 1992-1: 2004

INTERNAL COLUMN

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Project

Client

Location

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Project

Client

Location

chg

-

FB625

DATA

f_{ck} N/mm²

32

f_{yk} N/mm²

500

RC Density

kN/m³

25

VALID DESIGN

Class

B

Legs

Stud

z dir

RC Density

kN/m³

25

normal weight

T1

DIMENSIONS

Slab

h

mm

200

Cov

mm

35

A

mm

60

C

mm

N/A

E

mm

0

B

mm

60

D

mm

N/A

F

mm

0

v(L1/L2)

No

G

mm

0

H

mm

0

ULT LOADING

V_{ed}

kN

90

Edge w

kN/m

N/A

u

kN/m²

0.0

Axial

↔

kN/m

0

↓

kN/m

0

SLAB

z dir

10

y dir

12

dia @

200

ctr

dz

160

mm

Asz

mm²/m

393

in

B + 6d

%pz

0.245

dia @

200

ctr

dy

150

mm

Asy

mm²/m

393

in

A + 6d

%py

0.262

Spur Layout

%p <= 2

Yes

d

155

mm

%p

0.253

RESULTS

1.5Aswfyd_{ef} / SrU1

6.494

0.75vRd,c

=

0.420

N/mm²

Uout

xd

0.98

V_{Ed} = β(V_{Ed} - UDL)

=

104

kN

At

2.00

x d

vRd,c

=

0.560

N/mm²

vRd,cs

=

6.914

At column face, vEd

=

2.782

N/mm²

At

2.0

x d

vEd

=

0.305

N/mm²

vEd/vRd,c

=

0.545

vEd / vRd,c max

=

2.0

V_{E,out}

=

104

kN

Gross Uout

=

1192

mm

Gross U1

mm

2188

σcz & σcy

0.000

0.000

k1 σcp

0.000

V_{ed} Max

No legs

=

165

kN

Legs

330

No Legs

Leg Dia

20

Auto x d

0.5

8 Spur Perim

No

Control Perim

at

310

mm

HOLE DEDUCTION

By Interpolation & Extrapolation - See adjacent detailed check

Total Deduction at 2d

=

0

mm

Total Deduction at 4d

=

0

mm

Total Deduction at 6d

=

0

mm

Total Deduction at Uout at 0.98d

=

0

mm

Net U1

=

2188

-

0

=

2188

mm

Net Uout

=

1192

-

0

=

1192

mm

Perimeter at U1

Perimeter at Uout

Stress Cap Rd,c & Applied Stress Ed at Outer Perimeter x d From Face

Stress Rd,c & Ed

N/mm²

0

1

2

3

4

5

6

7

8

9

10

11

12

13

14

15

16

17

18

Deductions at 2d

Sides

0

0

mm

Quads

Distance 1 - 2

Distance 1 - 3

Deduction

Sides

Deductions at 4d

Sides

0

0

mm

Quads

Distance 1 - 2

Distance 1 - 3

Deduction

Sides

Deductions at 6d

Sides

0

0

mm

Quads

Distance 1 - 2

Distance 1 - 3

Deduction

Sides

Check Deductions at 0.98d

Sides

0

0

mm

Quads

Distance 1 - 2

Distance 1 - 3

Deduction

Sides

Project Birchwood, Hedge End

Client Glen Crump

Location Typical Edge Column



The Concrete Centre

Made by

ra

Date

14-Dec-2025

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#VALUE!

Checked

-

Revision

-

Job No

240510



PUNCHING SHEAR to BS EN 1992-1:2004

EDGE

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DATA

 f_{ck} N/mm²

32

 f_{yk} N/mm²

500

RC Density KN/m³

25

Class **B**
normal weight

Legs

T1

Bar

z dir

↔

VALID DESIGN

DIMENSIONS

Slab

h mm

200

Cov mm

35

A mm

60

C mm

N/A

E mm

G mm

0

B mm

60

D mm

240

F mm

H mm

0

 $v(L1/L2)$

Yes

ULT LOADING

 V_{ed} kN

103

Edge w kN/m

0.0

 u kN/m²

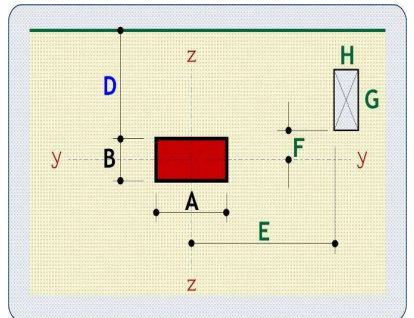
0.0

Axial ↔ kN/m

0

↓ kN/m

0

 β Using Factors =

1.400

braced, adj spans diff ≤ 25%

SLAB

z dir

10 12

dia @

100

ctrs dz

159.5

mm Asz mm²/m

958

in B + 3d

%pz 0.601

y dir

10 12

dia @

100

ctrs dy

147.5

mm Asy mm²/m

958

in A + 6d

%py 0.650

Spur Layout

All

%p ≤ 2

Yes

d 153.5 mm

%p 0.625

RESULTS

 $1.5A_{swfyd,ef} / S_{rU1}$

1.038

 $0.75vR_{d,c} =$

0.489

N/mm² $U_{out} \times d$

1.62

 $V_{E0} = \beta(V_{Ed} - UDL) =$

144

kN At

2.0

 $x \times d$ $vR_{d,c} =$

0.651

N/mm² $vR_{d,cs}$

1.527

At column face, $vEd =$

5.219

N/mm² At

2.0

 $x \times d$ $vEd =$

0.578

N/mm² $vEd/vR_{d,c}$

0.888

 $vEd / vR_{d,c} \max =$

2.0

 $V_{E,out} =$

144

kN Gross $b0.5,out$

1442

mm

Gross U1 mm

1624

 $\sigma_{cz} \text{ \& } \sigma_{cy}$

0.000

0.000

k1 σ_{cp}

0.000

 $V_{ed} \max$

No legs =

116

kN Legs

232

No Legs

Control Perim at 535 mm

Leg Dia

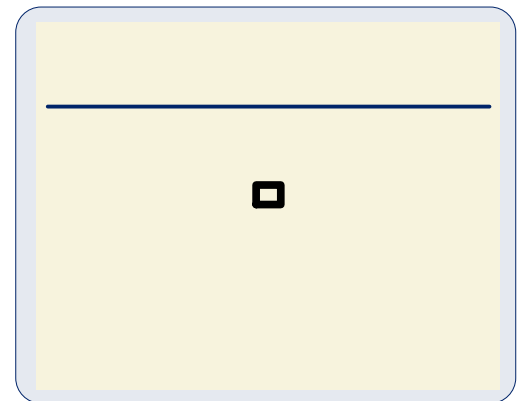
Auto

Auto $x \times d$

0.5

5 Spur Perim

No



HOLE DEDUCTION

Total Deduction at 2d = 0 mm

Total Deduction at 4d = 0 mm

Total Deduction at 6d = 0 mm

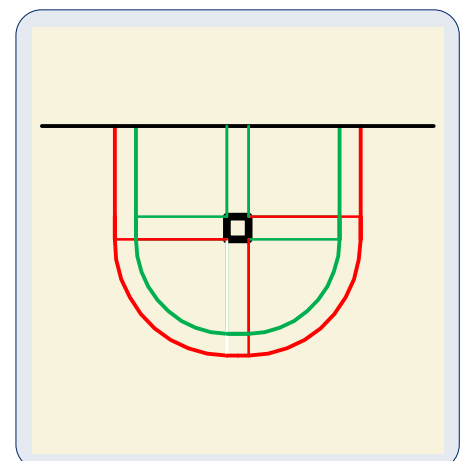
Total Deduction at U_{out} at 1.62d = 0 mm

Net U1 = 1624 - 0 = 1624 mm

Net Uout = 1442 - 0 = 1442 mm

Perimeter at U1

Perimeter at Uout



Project Spreadsheets

Client Advisory Group

Location Column B2



The Concrete Centre

The Concrete Centre

Made by

ra

Date

14-Dec-2025

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chg

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-

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FB625

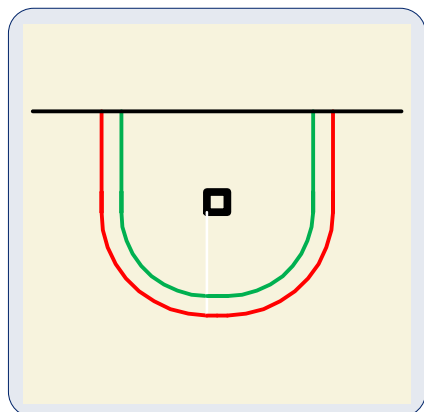


PUNCHING SHEAR to BS EN 1992-1: 2004

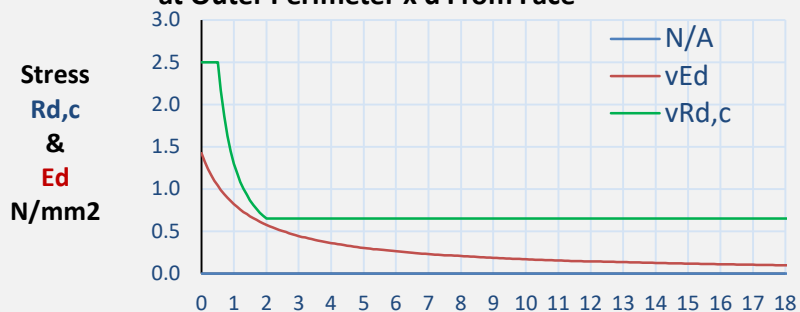
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EDGE
COLUMN



Stress Cap $R_{d,c}$ & Applied Stress E_d
at Outer Perimeter x d From Face



Deductions at 2d

Sides 0 0 mm

Quads

Distance 1 - 2
Distance 1 - 3
Deduction

Sides

Deductions at 4d

Sides 0 0 mm

Quads

Distance 1 - 2
Distance 1 - 3
Deduction

Sides

Deductions at 6d

Sides 0 0 mm

Quads

Distance 1 - 2
Distance 1 - 3
Deduction

Sides

Check at 1.62d

Sides 0 0 mm

Quads

Distance 1 - 2
Distance 1 - 3
Deduction

Sides

